

## 22. PALEOMAGNETISM OF SPECIMENS FROM LEG 3 OF THE DEEP SEA DRILLING PROJECT<sup>1</sup>

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Leg 3 of the Deep Sea Drilling Project provided the first opportunity to look at actual sections of paleomagnetic stratigraphy for parts of the Lower Miocene, Upper Oligocene and the Cretaceous-Tertiary boundary. This was because of the much improved core recovery which included several long sections of continuous core, and to a greater density of samples than was recovered from either Leg 1 or 2.

Samples were treated in the same manner as those for the two previous legs. All samples were measured at the natural remanent magnetization (NRM), and were cleaned in a field of 50 oersteds. The summary data is given in Table 1.

An A-F demagnetization curve for fields up to 200 oersteds was plotted on a pilot sample from each hole. These curves can be seen in Figures 1 through 13. Most samples that are of easily measurable intensity are seen to be partially stable. Sample 3-13A-5-1, however, is extremely weak ( $10^{-8}$  emu/gm), which probably is the reason for the strange behavior of this sample.

Figures 14 through 20 illustrate attempts to form a magnetic stratigraphy for the more densely sampled sections. Normal sections (which have a negative inclination for the southern latitude Sites 14 through 21) are indicated in black and reversed sections are shown in diagonal strips. The sections that were not cored are white. Actual sample points are indicated by arrows to the left of each diagram.

Problems in correlation occur both within individual sites and between different sites. In two sites (Sites 15 and 19) paleontologists recognized the problem of repeated sections found in sequential cores. Thus the paleomagnetic data from Hole 15, Core 9, Hole 19, Core 8 and Hole 19, Core 9 should be disregarded.

Another problem occurs in correlations between adjacent holes at the same site. In Site 20, for instance, the Upper Oligocene sections of Hole 20B and Hole 20C

seem to be out of phase. In Site 17, although the polarity overlap of Holes 17A and 17B in the Upper Oligocene seems pretty good, the inclination values are quite different. In Hole 17A, Core 4 (from 96 to 103 meters) the inclinations are extremely high—from 65 to 75 degrees—while in Hole 17B, Core 1 and 2, the inclination values are low.

Correlation between sites is extremely difficult due to the widely differing sedimentation rates and imprecise dating. An attempt can be made to correlate only when a distinct paleontological boundary or a distinct, synchronous lithologic unit was cored more than once. There are three opportunities present: the Upper Oligocene-Lower Oligocene boundary in Sites 19 and 20, the Eocene-Lower Oligocene boundary in Sites 14 and 19; and, several corings of the Maxwell Chalk Layer.

The Lower Oligocene-Eocene boundary occurs at Site 19 at 79 meters and at Site 14 at the very bottom of the hole. In both cases the boundary occurs in a reversely magnetized section of core with a normally magnetized section above. The Upper Oligocene/Lower Oligocene boundary in Hole 14 at 87 meters and Hole 20A at 18 meters also occurs in reversely magnetized sediments. Thus in both of these cases the paleontology and paleomagnetics are mutually supporting.

The Maxwell Chalk occurs in six separate holes. In Holes 17B, 20B and 22 it occurs in a normally magnetized section of core; while at Holes 14, 17A and 19, it occurs in reversely magnetized sections of core. The reversed section at Hole 14 rests on only one measurement, and in Hole 17A on two measurements. The sampled sections in both of these holes are short. In only Hole 19 is the reversely magnetized section of core associated with the Maxwell Chalk well established, and in this hole the chalk is .5 centimeter thick so that miscorrelation is possible. The most reliable measurements are probably from Site 22 where a thick section of chalk was cored. Here a normal direction is observed. Therefore, the most reasonable interpretation is that the magnetic field of the earth was normal at the time of deposition of the Maxwell Chalk. This interpretation, however, is by no means unambiguous.

The other significant paleontological boundary that was cored during Leg 3 was the Cretaceous-Tertiary

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boundary seen in Hole 20C. The extremely close sampling interval here allows for a well documented view across the boundary which seems to have occurred at a time when the magnetic field of the earth was reversed. There are two anomalous, normally magnetized samples that occur in the section. The first—20C-6-4, 112 centimeters—is a sample of a reworked Cretaceous clump which is found in Paleocene sediments just above the boundary; and, the other—20C-6-5, 0-2 centimeters—is taken from the very top of a section and thus is very possibly disturbed. Although based on only one section of core, it seems most likely that the

Cretaceous-Tertiary boundary occurred while the field of the earth remained reversed.

The outstanding results of the Leg 3 paleomagnetic studies can be summarized as follows:

1. Sediments of both polarities occur in all the geological epochs of the Cenozoic and into the Upper Cretaceous.
2. The Upper Oligocene/Lower Oligocene boundary, the Oligocene/Eocene boundary and the Tertiary/Cretaceous boundary occur at times in which the magnetic field of the earth was reversed.

**TABLE I**  
**Summary of Magnetic Data**

The data are presented in order by site. Sample numbers are given as hole number, core, section, and then the starting depth of the sample in centimeters.

Magnetic directions and intensities in emu/gm are given for each sample at NRM, and followed by the A-F demagnetization in a field of 50 oersteds. Note that a negative (positive) inclination indicates a normal (reversed) field direction for sites in the southern hemisphere (Sites 14 through 22); the opposite is true for Site 13 in the northern hemisphere.

An asterisk beside a sample number indicates that it is used as a pilot sample for the site and an A-F demagnetization curve has been completed. These are presented in Figures 1 through 13.

Hole	Core	Section	Sampled at (cm)	NRM			50 oersted		
				Decl.	Incl.	Intensity emu/gm	Decl.	Incl.	Intensity emu/gm
13A	2	1	114	202.7	-68.8	$0.1136 \times 10^{-6}$	56.3	-78.6	$0.6949 \times 10^{-7}$
13A	3	1	113	132.1	-1.3	$0.3500 \times 10^{-6}$	123.5	67.1	$0.9303 \times 10^{-6}$
13A	3	2	11	225.7	4.4	$0.3656 \times 10^{-6}$	208.1	25.2	$0.2566 \times 10^{-6}$
13A	3	2	50	241.1	-23.8	$0.2675 \times 10^{-6}$	223.6	-21.5	$0.3069 \times 10^{-6}$
13A	3	4	50	215.7	-5.9	$0.2919 \times 10^{-6}$	63.9	29.1	$0.3174 \times 10^{-6}$
13A	5	1	49.51	222.7	-36.3	$0.8200 \times 10^{-7}$	240.6	-37.3	$0.8616 \times 10^{-7}$
14A	1	1	99	192.3	-11.3	$0.5723 \times 10^{-5}$	218.4	-40.3	$0.1726 \times 10^{-5}$
14A	1	3	50.2	192.1	26.4	$0.6244 \times 10^{-5}$	188.9	30.4	$0.2046 \times 10^{-5}$
14A	1	5	39	171.5	-9.6	$0.8470 \times 10^{-5}$	161.8	-21.1	$0.2174 \times 10^{-5}$
14A	1	6	49	175.2	13.6	$0.6781 \times 10^{-5}$	207.0	54.6	$0.2915 \times 10^{-5}$
14	2	1	120	170.3	10.1	$0.4595 \times 10^{-5}$	171.4	-12.0	$0.1486 \times 10^{-5}$
14	2	2	48	169.0	1.3	$0.2717 \times 10^{-5}$	162.9	-11.8	$0.8346 \times 10^{-6}$
14	2	3	65	44.3	-25.9	$0.1829 \times 10^{-4}$	31.3	-19.0	$0.1841 \times 10^{-4}$
14	2	4	50	203.6	-14.4	$0.4833 \times 10^{-5}$	235.5	-28.5	$0.2000 \times 10^{-5}$
14	2	5	52	216.2	-7.0	$0.3208 \times 10^{-5}$	246.6	-15.1	$0.1809 \times 10^{-5}$
14	3	2	52	188.1	-34.5	$0.3942 \times 10^{-5}$	207.4	-54.7	$0.2064 \times 10^{-5}$

TABLE 1—Continued

Hole	Core	Section	Sampled at (cm)	NRM			50 oersted		
				Decl.	Incl.	Intensity emu/gm	Decl.	Incl.	Intensity emu/gm
14	3	3	50	196.1	7.5	$0.3763 \times 10^{-5}$	148.0	6.3	$0.1195 \times 10^{-5}$
14	3	4	50	166.6	-10.0	$0.3661 \times 10^{-5}$	181.1	-14.6	$0.1023 \times 10^{-5}$
14	4	1	36	105.5	6.5	$0.6383 \times 10^{-5}$	106.4	5.4	$0.3801 \times 10^{-5}$
14	5	2	100	170.7	-22.2	$0.2399 \times 10^{-5}$	137.0	-30.4	$0.1106 \times 10^{-5}$
14	5	3	56	201.7	25.9	$0.1254 \times 10^{-5}$	286.1	-20.8	$0.4556 \times 10^{-6}$
14	5	4	50	222.9	31.1	$0.1960 \times 10^{-5}$	259.3	54.0	$0.1136 \times 10^{-5}$
14	6	3	50	165.0	15.8	$0.1833 \times 10^{-5}$	148.1	47.7	$0.8679 \times 10^{-6}$
14	6	4	50	195.3	15.0	$0.1824 \times 10^{-5}$	210.8	75.7	$0.1535 \times 10^{-5}$
14	6	5	50	177.0	53.9	$0.3287 \times 10^{-5}$	213.0	67.5	$0.2231 \times 10^{-5}$
14	6	6	50	171.6	12.6	$0.2329 \times 10^{-5}$	143.7	30.0	$0.8088 \times 10^{-6}$
14	7	1	50	145.7	42.4	$0.3654 \times 10^{-5}$	122.4	47.7	$0.2965 \times 10^{-5}$
14	7	2	50	297.2	45.4	$0.4576 \times 10^{-5}$	321.7	37.8	$0.3790 \times 10^{-5}$
14	7	3	50	189.2	19.7	$0.2781 \times 10^{-5}$	193.8	52.0	$0.8881 \times 10^{-6}$
14	7	4	50	154.2	-20.8	$0.2041 \times 10^{-5}$	64.5	58.1	$0.1508 \times 10^{-5}$
14	7	5	100	156.0	26.3	$0.2820 \times 10^{-5}$	117.6	16.8	$0.1561 \times 10^{-5}$
14	7	6	9	145.5	32.2	$0.6908 \times 10^{-5}$	142.1	42.3	$0.5191 \times 10^{-5}$
14	8	1	45	340.8	46.5	$0.1979 \times 10^{-3}$	344.3	46.3	$0.1674 \times 10^{-3}$
14	8	5	50	198.6	52.3	—	182.2	53.7	—
14	9	2	50	301.1	-10.0	$0.3738 \times 10^{-3}$	303.3	-0.0	$0.3353 \times 10^{-3}$
14	9	4	100	172.5	-10.1	$0.2732 \times 10^{-3}$	210.7	-48.3	$0.1513 \times 10^{-5}$
14	9	5	50	253.8	-32.8	$0.2017 \times 10^{-5}$	252.4	-52.5	$0.8186 \times 10^{-6}$
14	9	5	123	172.3	36.1	$0.2369 \times 10^{-5}$	119.7	10.7	$0.6354 \times 10^{-6}$
14	9	6	15	141.6	32.7	$0.5742 \times 10^{-5}$	133.3	40.2	$0.3818 \times 10^{-5}$
14	9	6	50	116.0	35.7	$0.7914 \times 10^{-5}$	109.4	44.2	$0.4906 \times 10^{-5}$
14	9	6	100	163.5	26.3	$0.2195 \times 10^{-5}$	103.4	66.3	$0.4901 \times 10^{-6}$
15	1	1	50	139.0	-68.1	$0.5962 \times 10^{-5}$	142.5	-73.1	$0.3079 \times 10^{-5}$
15	1	1	103	170.7	-28.3	—	138.3	-30.5	—
15	1	2	50	147.2	-73.2	$0.2303 \times 10^{-5}$	129.5	-65.9	$0.1129 \times 10^{-5}$
15	1	3	54	129.3	-15.7	$0.3462 \times 10^{-5}$	150.0	-35.1	$0.2071 \times 10^{-5}$

TABLE 1—Continued

Hole	Core	Section	Sampled at (cm)	NRM			50 oersted		
				Decl.	Incl.	Intensity emu/gm	Decl.	Incl.	Intensity emu/gm
15	1	5	33	213.5	22.9	$0.5437 \times 10^{-5}$	221.7	31.3	$0.3407 \times 10^{-5}$
15	1	5	54	235.9	34.0	$0.1290 \times 10^{-6}$	223.2	43.1	$0.8957 \times 10^{-5}$
15	1	6	18	168.6	-29.5	$0.2900 \times 10^{-5}$	171.8	-29.8	$0.1300 \times 10^{-5}$
15	1	6	50	136.5	12.7	$0.1345 \times 10^{-5}$	251.1	-24.2	$0.7126 \times 10^{-6}$
15	1	6	71	223.7	-4.1	—	231.9	-2.6	—
15	2	1	48	271.8	-9.9	$0.6661 \times 10^{-5}$	273.3	54.9	$0.2453 \times 10^{-5}$
15	2	4	107	208.4	17.5	$0.1980 \times 10^{-5}$	213.6	60.7	$0.7028 \times 10^{-6}$
15	2	5	48	78.0	-47.6	$0.6320 \times 10^{-5}$	60.2	-50.9	$0.1492 \times 10^{-5}$
15	2	5	100	142.9	25.0	—	53.8	32.9	—
15	2	6	48	77.1	-84.6	—	66.8	-48.0	—
15	2	6	105	164.2	33.2	—	148.1	43.3	—
15	3	1	52	269.3	-51.6	$0.6200 \times 10^{-5}$	266.7	-55.5	$0.2573 \times 10^{-5}$
15	3	1	100	173.3	-56.1	$0.5342 \times 10^{-5}$	168.3	-13.7	$0.8882 \times 10^{-6}$
15	3	2	50	263.9	46.4	$0.1257 \times 10^{-4}$	275.6	-47.0	$0.4048 \times 10^{-5}$
15	3	2	100	173.4	-31.6	$0.3896 \times 10^{-5}$	199.5	3.4	$0.1382 \times 10^{-5}$
15	3	4	43	93.9	26.5	—	86.2	32.4	—
15	3	4	100	160.8	7.1	$0.1759 \times 10^{-5}$	157.9	4.6	$0.3442 \times 10^{-6}$
15	3	5	100	185.0	13.7	$0.1921 \times 10^{-5}$	178.5	8.4	$0.8279 \times 10^{-6}$
15	3	6	9	172.7	-38.5	—	162.5	-45.2	—
15	4	1	23	240.5	50.0	—	282.9	53.7	—
15	4	1	55	65.8	-29.7	—	63.2	-22.2	—
15	4	1	98	202.4	37.4	—	119.4	78.0	—
15	4	2	50	170.6	-20.1	$0.3198 \times 10^{-5}$	162.9	18.4	$0.9421 \times 10^{-6}$
15	4	2	102	148.3	40.6	$0.7453 \times 10^{-6}$	72.4	31.7	$0.5487 \times 10^{-6}$
15	4	3	12	164.0	16.9	$0.9072 \times 10^{-6}$	22.1	43.4	$0.5503 \times 10^{-6}$
*15	4	3	41-3	143.9	10.4	$0.7885 \times 10^{-6}$	70.2	36.9	$0.4740 \times 10^{-6}$
15	4	4	54	173.9	0.5	$0.3061 \times 10^{-5}$	174.7	9.7	$0.1264 \times 10^{-5}$
15	4	4	100	211.6	-17.8	$0.1092 \times 10^{-5}$	66.8	-65.4	$0.4916 \times 10^{-6}$
15	4	5	12	130.7	13.1	$0.1017 \times 10^{-5}$	185.1	-8.4	$0.4905 \times 10^{-6}$

TABLE 1—Continued

Hole	Core	Section	Sampled at (cm)	NRM			50 oersted		
				Decl.	Incl.	Intensity emu/gm	Decl.	Incl.	Intensity emu/gm
15	4	5	100	236.3	38.4	$0.5856 \times 10^{-6}$	76.1	-1.0	$0.4802 \times 10^{-6}$
15	4	6	12	241.1	-13.2	$0.2963 \times 10^{-5}$	281.8	-16.3	$0.6265 \times 10^{-6}$
15	4	6	53	203.5	2.2	$0.5402 \times 10^{-5}$	211.7	-6.6	$0.1770 \times 10^{-5}$
15	4	6	100	230.9	-8.0	—	204.3	-18.5	—
15	5	1	11	193.0	-67.9	$0.1452 \times 10^{-4}$	236.7	-10.9	$0.6899 \times 10^{-6}$
15	5	1	60	196.6	2.3	$0.1349 \times 10^{-4}$	176.5	44.5	$0.3330 \times 10^{-5}$
15	5	1	100	228.7	-6.2	$0.6351 \times 10^{-5}$	305.2	18.0	$0.1089 \times 10^{-5}$
15	5	2	45	169.4	-11.0	$0.3486 \times 10^{-5}$	206.4	-0.8	$0.2172 \times 10^{-5}$
15	5	2	100	197.4	-14.1	$0.3478 \times 10^{-5}$	120.7	21.8	$0.1192 \times 10^{-5}$
15	5	3	12	194.2	-14.0	—	85.3	12.6	—
15	5	3	52	192.5	-14.3	$0.4447 \times 10^{-5}$	259.0	-5.3	$0.1787 \times 10^{-5}$
15	5	3	100	169.3	0.9	$0.2689 \times 10^{-5}$	—	—	—
15	5	4	9	205.4	-16.9	$0.3224 \times 10^{-5}$	188.0	-1.9	$0.1113 \times 10^{-5}$
15	5	4	48	159.8	48.9	$0.5072 \times 10^{-5}$	142.9	22.7	$0.1277 \times 10^{-5}$
15	5	4	100	233.1	48.8	$0.2788 \times 10^{-5}$	58.2	62.6	$0.1553 \times 10^{-5}$
15	5	5	11	142.9	-26.0	—	—	—	—
15	5	5	51	249.3	32.2	$0.2035 \times 10^{-4}$	257.7	53.4	$0.3924 \times 10^{-5}$
15	5	6	11	194.4	10.5	$0.3200 \times 10^{-5}$	121.7	89.5	$0.1193 \times 10^{-3}$
15	5	6	100	162.0	57.1	—	291.5	66.4	—
15	6	1	11	212.8	12.8	$0.1550 \times 10^{-4}$	247.3	39.9	$0.5862 \times 10^{-5}$
15	6	1	67	201.5	-7.4	$0.1839 \times 10^{-4}$	180.3	45.4	$0.5720 \times 10^{-5}$
15	6	2	62	191.1	15.7	—	163.2	15.4	—
15	6	3	2	190.9	20.7	$0.2669 \times 10^{-4}$	105.9	23.1	$0.2289 \times 10^{-5}$
15	6	3	11	166.0	-59.9	$0.2000 \times 10^{-4}$	212.9	8.5	$0.2619 \times 10^{-5}$
15	6	3	52	210.1	-16.8	$0.2010 \times 10^{-4}$	140.1	17.8	$0.4387 \times 10^{-5}$
15	6	3	100	214.9	-31.1	$0.1350 \times 10^{-4}$	172.7	13.2	$0.3639 \times 10^{-5}$
15	6	4	2	194.7	19.2	$0.3250 \times 10^{-5}$	—	—	—
15	6	4	11	155.9	30.1	$0.1027 \times 10^{-4}$	155.4	55.4	$0.2611 \times 10^{-5}$
15	6	4	52	196.7	11.4	$0.1907 \times 10^{-4}$	210.0	9.6	$0.4763 \times 10^{-5}$

TABLE 1—Continued

Hole	Core	Section	Sampled at (cm)	NRM			50 oersted		
				Decl.	Incl.	Intensity emu/gm	Decl.	Incl.	Intensity emu/gm
15	6	4	101	156.2	-12.3	$0.9342 \times 10^{-5}$	220.1	-29.1	$0.2330 \times 10^{-5}$
15	6	4	108	328.3	-67.7	$0.2256 \times 10^{-5}$	202.3	-9.2	$0.3706 \times 10^{-5}$
15	6	5	11	165.1	65.2	$0.4214 \times 10^{-5}$	80.7	61.4	$0.2841 \times 10^{-5}$
15	6	5	51	196.6	19.2	$0.5663 \times 10^{-5}$	168.2	52.8	$0.2725 \times 10^{-5}$
15	6	5	100	184.7	-4.9	$0.4503 \times 10^{-5}$	14.7	-82.1	$0.1373 \times 10^{-5}$
15	6	6	2	223.0	-34.3	$0.7748 \times 10^{-5}$	252.1	-77.1	$0.6524 \times 10^{-5}$
15	6	6	10	145.9	49.2	$0.6753 \times 10^{-5}$	120.0	64.8	$0.3303 \times 10^{-5}$
15	6	6	52	182.6	-23.2	$0.6837 \times 10^{-5}$	200.2	-15.9	$0.2396 \times 10^{-5}$
15	6	6	100	186.8	21.5	$0.7264 \times 10^{-5}$	196.9	75.3	$0.3174 \times 10^{-5}$
15	7	1	11	290.8	-59.4	$0.3056 \times 10^{-5}$	315.8	-47.1	$0.2749 \times 10^{-5}$
15	7	1	52	157.0	-22.6	$0.5928 \times 10^{-5}$	163.9	-43.3	$0.2687 \times 10^{-5}$
15	7	1	100	328.8	-64.4	$0.7652 \times 10^{-5}$	31.0	-46.4	$0.5480 \times 10^{-5}$
15	7	2	13	246.2	-31.6	$0.1027 \times 10^{-4}$	248.9	-45.8	$0.2688 \times 10^{-5}$
15	7	2	50	209.7	-29.1	$0.6387 \times 10^{-5}$	215.9	-48.1	$0.3062 \times 10^{-5}$
15	7	2	100	172.7	-41.1	—	226.7	-29.6	—
15	7	2	100	199.4	20.1	—	239.8	52.2	—
15	7	3	12	140.1	47.0	—	128.6	69.5	—
15	7	3	48	183.9	-11.1	$0.2816 \times 10^{-5}$	246.1	12.1	$0.4510 \times 10^{-6}$
15	7	4	11	198.5	-6.1	$0.3631 \times 10^{-5}$	215.4	-11.5	$0.2199 \times 10^{-5}$
15	7	4	52	282.5	-81.6	$0.6367 \times 10^{-5}$	287.2	-70.0	$0.4168 \times 10^{-5}$
15	7	4	100	228.6	-28.3	$0.3917 \times 10^{-5}$	279.0	-25.2	$0.3128 \times 10^{-5}$
15	7	5	11	131.8	2.8	$0.4437 \times 10^{-5}$	85.8	-29.1	$0.1488 \times 10^{-5}$
15	7	5	48	205.6	-42.9	$0.8769 \times 10^{-5}$	199.6	-57.6	$0.1695 \times 10^{-5}$
15	7	5	100	206.2	20.2	$0.3967 \times 10^{-5}$	241.3	-6.9	$0.2317 \times 10^{-5}$
15	7	6	2	165.7	6.9	$0.4983 \times 10^{-5}$	250.6	75.0	$0.1448 \times 10^{-5}$
15	7	6	12	190.2	-55.0	$0.8196 \times 10^{-5}$	252.1	-58.5	$0.2823 \times 10^{-5}$
15	7	6	54	161.0	0.8	$0.5677 \times 10^{-5}$	95.7	59.8	$0.1712 \times 10^{-5}$
15	7	6	102	206.4	58.5	$0.5355 \times 10^{-5}$	257.0	55.9	$0.3972 \times 10^{-5}$
15	8	2	50	153.7	5.1	$0.3590 \times 10^{-5}$	129.6	-7.6	$0.1407 \times 10^{-5}$

TABLE 1—Continued

Hole	Core	Section	Sampled at (cm)	NRM			50 oersted		
				Decl.	Incl.	Intensity emu/gm	Decl.	Incl.	Intensity emu/gm
15	8	3	2	266.3	1.1	$0.3253 \times 10^{-4}$	84.8	-68.4	$0.3618 \times 10^{-6}$
15	8	3	13	157.5	-19.1	$0.1978 \times 10^{-5}$	97.1	-44.7	$0.4560 \times 10^{-6}$
15	8	3	100	164.9	-71.8	$0.5178 \times 10^{-5}$	186.1	-27.0	$0.4282 \times 10^{-6}$
15	8	4	2	210.0	-1.3	$0.3195 \times 10^{-5}$	299.0	-30.2	$0.1733 \times 10^{-6}$
15	8	4	12	152.2	-4.3	$0.1156 \times 10^{-5}$	335.5	-61.2	$0.2752 \times 10^{-6}$
15	8	4	48	147.3	-7.7	$0.3507 \times 10^{-5}$	66.1	-48.1	$0.6748 \times 10^{-6}$
15	8	4	103	182.5	-23.7	$0.1916 \times 10^{-5}$	170.5	-30.6	$0.3895 \times 10^{-6}$
15	8	5	2	132.9	-46.7	$0.3284 \times 10^{-5}$	225.9	-39.0	$0.4154 \times 10^{-6}$
15	8	5	11	128.6	-14.9	$0.2100 \times 10^{-5}$	58.8	-29.9	$0.7076 \times 10^{-6}$
15	8	5	50	222.0	-4.7	—	214.8	-22.4	—
15	8	5	100	161.6	-24.9	$0.1849 \times 10^{-5}$	217.3	-20.5	$0.4781 \times 10^{-6}$
15	8	6	13	160.7	-21.4	—	169.8	-8.3	—
15	8	6	51	139.3	-7.8	$0.4062 \times 10^{-5}$	246.6	-30.3	$0.9087 \times 10^{-6}$
15	9	1	48	175.6	20.5	$0.2608 \times 10^{-5}$	172.8	20.2	$0.8032 \times 10^{-6}$
15	9	1	110	226.0	-48.5	$0.6513 \times 10^{-4}$	237.5	-46.4	$0.6214 \times 10^{-4}$
15	9	2	52	166.3	-17.4	$0.5339 \times 10^{-5}$	150.4	2.0	$0.1330 \times 10^{-5}$
15	9	2	105	201.8	8.5	$0.4102 \times 10^{-4}$	201.6	5.7	$0.3490 \times 10^{-4}$
15	9	3	2	142.4	13.9	$0.4945 \times 10^{-5}$	104.0	49.1	$0.1290 \times 10^{-5}$
15	9	3	51	203.1	-3.8	$0.4534 \times 10^{-5}$	196.5	-18.3	$0.1122 \times 10^{-5}$
15	9	3	104	171.0	-16.3	$0.1698 \times 10^{-5}$	299.7	-53.7	$0.7320 \times 10^{-6}$
15	9	4	52	160.7	19.7	$0.6894 \times 10^{-5}$	149.1	46.7	$0.3267 \times 10^{-5}$
15	9	4	100	123.3	59.1	$0.7020 \times 10^{-5}$	25.2	60.5	$0.4842 \times 10^{-5}$
15	9	5	2	226.8	35.4	$0.6258 \times 10^{-5}$	250.4	37.4	$0.3061 \times 10^{-5}$
15	9	5	11	203.2	-43.2	$0.6214 \times 10^{-5}$	222.9	49.1	$0.4346 \times 10^{-5}$
15	9	5	53	141.4	-49.5	$0.3455 \times 10^{-5}$	100.8	-70.6	$0.2745 \times 10^{-5}$
15	9	5	100	195.9	24.4	$0.3026 \times 10^{-5}$	237.6	-46.4	$0.1861 \times 10^{-5}$
15	9	6	10	116.6	-38.6	$0.2890 \times 10^{-5}$	70.4	-54.5	$0.2102 \times 10^{-5}$
15	9	6	51	178.7	-27.6	—	174.9	-38.8	—
16	1	1	12	357.4	2.8	$0.4924 \times 10^{-5}$	341.9	9.3	$0.2067 \times 10^{-5}$

TABLE 1—Continued

Hole	Core	Section	Sampled at (cm)	NRM			50 oersted		
				Decl.	Incl.	Intensity emu/gm	Decl.	Incl.	Intensity emu/gm
16	1	1	48	245.8	11.2	$0.7603 \times 10^{-5}$	268.3	6.2	$0.6597 \times 10^{-5}$
16	1	1	100	140.5	7.7	$0.1004 \times 10^{-5}$	51.4	-23.1	$0.6909 \times 10^{-6}$
16	1	2	100	0.1	-2.6	—	348.6	-42.1	—
16	2	6	2	171.7	29.8	$0.2662 \times 10^{-5}$	167.0	38.4	$0.1209 \times 10^{-5}$
16	2	6	11	122.7	17.5	$0.1233 \times 10^{-5}$	94.5	-33.0	$0.6081 \times 10^{-6}$
*16	2	6	50-2	211.7	-21.2	$0.1579 \times 10^{-5}$	228.8	43.2	$0.5712 \times 10^{-6}$
16	4	1	52	198.7	4.7	$0.3380 \times 10^{-5}$	219.4	15.6	$0.1781 \times 10^{-5}$
16	4	1	100	153.7	0.6	$0.2270 \times 10^{-5}$	147.4	-15.4	$0.7613 \times 10^{-6}$
16	4	2	11	172.4	0.3	$0.2204 \times 10^{-5}$	173.3	-18.9	$0.1470 \times 10^{-5}$
16	4	2	100	134.2	8.3	$0.1035 \times 10^{-5}$	190.4	21.8	$0.2976 \times 10^{-6}$
16	4	3	13	194.7	35.4	—	216.0	32.2	—
16	4	3	54	168.4	27.2	$0.2079 \times 10^{-5}$	159.0	41.7	$0.1278 \times 10^{-5}$
16	4	3	100	163.5	-0.8	$0.1327 \times 10^{-5}$	185.5	12.6	$0.3080 \times 10^{-6}$
16	4	4	10	165.4	29.4	$0.8978 \times 10^{-6}$	152.1	41.4	$0.5042 \times 10^{-6}$
16	4	4	50	175.6	-11.7	$0.2217 \times 10^{-5}$	201.1	-3.7	$0.1398 \times 10^{-5}$
16	4	4	100	171.6	25.3	$0.1378 \times 10^{-5}$	175.4	19.7	$0.8010 \times 10^{-6}$
16	4	5	12	160.7	-3.2	$0.1008 \times 10^{-5}$	163.3	10.8	$0.5053 \times 10^{-6}$
16	4	5	50	178.4	-23.9	$0.2510 \times 10^{-5}$	170.4	-32.0	$0.1202 \times 10^{-5}$
16	4	5	100	183.1	-4.7	$0.1455 \times 10^{-5}$	177.7	-12.1	$0.7156 \times 10^{-6}$
17	1	1	53	175.6	22.0	$0.3938 \times 10^{-5}$	186.1	36.3	$0.1232 \times 10^{-5}$
17	1	2	50	197.9	-14.8	$0.4197 \times 10^{-5}$	183.4	-11.7	$0.1504 \times 10^{-5}$
17	1	4	50	182.0	3.7	$0.2552 \times 10^{-5}$	92.1	-1.9	$0.1245 \times 10^{-4}$
17	1	5	50	156.4	-4.6	$0.3576 \times 10^{-5}$	133.8	-8.7	$0.8343 \times 10^{-6}$
17	2	1	23	180.9	28.5	$0.1361 \times 10^{-5}$	172.4	56.2	$0.9210 \times 10^{-6}$
17	2	1	52	236.7	64.2	$0.1565 \times 10^{-3}$	240.9	63.1	$0.1451 \times 10^{-3}$
17	2	2	50	231.1	49.4	$0.1667 \times 10^{-4}$	235.8	35.9	$0.1159 \times 10^{-4}$
17	2	2	100	175.4	11.2	$0.8570 \times 10^{-6}$	174.4	18.7	$0.3644 \times 10^{-6}$
17	2	3	13	164.6	-20.7	$0.1451 \times 10^{-5}$	152.5	-38.7	$0.6142 \times 10^{-6}$
*17	2	3	54-6	147.9	-4.9	$0.5882 \times 10^{-6}$	154.9	-37.8	$0.2024 \times 10^{-6}$

TABLE 1—Continued

Hole	Core	Section	Sampled at (cm)	NRM			50 oersted		
				Decl.	Incl.	Intensity emu/gm	Decl.	Incl.	Intensity emu/gm
17	2	3	99	160.5	-20.5	$0.1114 \times 10^{-5}$	157.3	-30.5	$0.3941 \times 10^{-6}$
17	2	4	14	129.9	-2.9	$0.8327 \times 10^{-6}$	106.9	-14.0	$0.2134 \times 10^{-6}$
17	2	4	50	158.7	-8.0	$0.6165 \times 10^{-6}$	34.2	26.2	$0.2861 \times 10^{-6}$
17	2	4	114	202.3	-6.2	$0.4343 \times 10^{-6}$	179.5	-0.4	$0.4111 \times 10^{-5}$
17	2	5	40	92.8	38.3	—	47.1	37.2	—
17	2	5	100	160.3	44.7	$0.4084 \times 10^{-6}$	132.1	-56.6	$0.2466 \times 10^{-6}$
17	2	6	13	162.4	3.1	$0.2772 \times 10^{-6}$	126.8	-41.7	$0.1628 \times 10^{-6}$
17	2	6	50	178.0	-13.2	$0.2779 \times 10^{-5}$	170.9	-29.7	$0.5452 \times 10^{-6}$
17A	1	1	50	184.0	18.0	$0.6540 \times 10^{-5}$	182.9	25.9	$0.2547 \times 10^{-5}$
17A	1	1	100	164.8	1.0	$0.5600 \times 10^{-5}$	198.7	2.2	$0.1752 \times 10^{-5}$
17A	1	2	12	194.3	-21.5	$0.3233 \times 10^{-5}$	201.8	-40.2	$0.9652 \times 10^{-6}$
17A	1	2	50	159.6	11.4	$0.6549 \times 10^{-5}$	127.3	22.7	$0.2334 \times 10^{-5}$
17A	1	3	51	215.0	-43.6	$0.5034 \times 10^{-5}$	134.4	-76.5	$0.3095 \times 10^{-5}$
17A	1	4	50	137.6	-43.4	$0.1147 \times 10^{-4}$	111.7	13.8	$0.2156 \times 10^{-5}$
17A	1	4	100	189.5	-4.8	$0.5328 \times 10^{-5}$	88.6	-4.1	$0.1180 \times 10^{-5}$
17A	1	5	7	192.5	-30.1	$0.6126 \times 10^{-5}$	13.6	-43.1	$0.1133 \times 10^{-5}$
17A	1	5	50	138.5	36.4	$0.1150 \times 10^{-4}$	77.4	-24.6	$0.1833 \times 10^{-5}$
17A	1	5	100	186.1	16.2	$0.4999 \times 10^{-5}$	131.1	63.3	$0.7969 \times 10^{-6}$
17A	1	6	17	204.5	-10.1	$0.4257 \times 10^{-5}$	213.6	-30.3	$0.1435 \times 10^{-5}$
17A	2	1	69	177.4	-1.9	$0.8709 \times 10^{-5}$	120.4	-13.0	$0.1778 \times 10^{-5}$
17A	2	2	1	186.5	-43.2	$0.2578 \times 10^{-5}$	273.9	-78.4	$0.2696 \times 10^{-5}$
17A	2	2	100	184.8	-5.7	—	201.1	-31.1	—
17A	2	3	12	184.6	-13.3	—	246.5	-55.1	—
17A	2	4	12	191.0	4.6	$0.3676 \times 10^{-5}$	205.2	-24.8	$0.9814 \times 10^{-6}$
*17A	2	4	50-2	189.5	-17.7	$0.4022 \times 10^{-5}$	196.2	-34.8	$0.1065 \times 10^{-5}$
17A	2	4	100	234.2	31.8	$0.3580 \times 10^{-5}$	301.7	58.7	$0.2548 \times 10^{-5}$
17A	2	5	2	174.5	31.7	$0.3786 \times 10^{-5}$	153.2	50.2	$0.1806 \times 10^{-5}$
17A	2	5	62	182.8	-10.7	$0.4996 \times 10^{-5}$	220.9	-37.3	$0.1572 \times 10^{-5}$

TABLE 1—Continued

Hole	Core	Section	Sampled at (cm)	NRM			50 oersted		
				Decl.	Incl.	Intensity emu/gm	Decl.	Incl.	Intensity emu/gm
17A	2	5	100	181.0	18.8	$0.1580 \times 10^{-5}$	124.1	53.0	$0.7653 \times 10^{-6}$
17A	2	6	19	238.5	-28.8	$0.2117 \times 10^{-5}$	257.7	-37.7	$0.9664 \times 10^{-6}$
17A	2	6	50	174.3	-7.8	$0.4682 \times 10^{-5}$	169.3	-19.9	$0.1210 \times 10^{-5}$
17A	2	6	100	181.5	-12.9	$0.1838 \times 10^{-5}$	157.7	-61.6	$0.3445 \times 10^{-6}$
17A	3	1	53	207.3	19.4	$0.1862 \times 10^{-5}$	220.7	26.3	$0.8543 \times 10^{-6}$
17A	3	1	100	162.8	19.9	$0.1734 \times 10^{-5}$	161.8	15.8	$0.7381 \times 10^{-6}$
17A	4	2	8	182.6	0.8	$0.1088 \times 10^{-5}$	146.3	-63.8	$0.2035 \times 10^{-6}$
17A	4	2	50	196.6	-37.6	$0.3516 \times 10^{-5}$	240.1	-79.9	$0.1624 \times 10^{-5}$
17A	4	2	75	117.3	-55.8	$0.6680 \times 10^{-5}$	63.3	-65.0	$0.4908 \times 10^{-5}$
17A	4	2	100	169.1	-47.9	$0.4544 \times 10^{-5}$	156.1	-72.5	$0.2652 \times 10^{-5}$
17A	4	6	6	196.0	17.9	$0.9800 \times 10^{-6}$	197.7	50.6	$0.3041 \times 10^{-6}$
17A	4	6	50	182.8	-4.9	$0.2773 \times 10^{-5}$	201.5	-27.0	$0.5408 \times 10^{-6}$
17A	4	6	75	199.3	-22.5	$0.4828 \times 10^{-5}$	176.3	-50.6	$0.2191 \times 10^{-5}$
17A	4	6	105	51.0	31.6	$0.4195 \times 10^{-6}$	43.8	13.2	$0.6051 \times 10^{-6}$
17B	1	1	16	124.9	-5.5	$0.1568 \times 10^{-5}$	62.9	5.7	$0.1129 \times 10^{-5}$
17B	1	1	50	195.9	2.2	$0.5421 \times 10^{-5}$	220.0	16.2	$0.1761 \times 10^{-5}$
17B	1	1	100	168.8	-33.1	$0.2557 \times 10^{-5}$	199.1	-25.9	$0.7112 \times 10^{-6}$
17B	1	2	2	203.8	-31.1	$0.3741 \times 10^{-5}$	203.6	-39.8	$0.1417 \times 10^{-5}$
17B	1	2	50	213.8	-12.2	$0.4359 \times 10^{-5}$	263.9	-33.7	$0.2016 \times 10^{-5}$
17B	1	2	100	174.7	-33.9	$0.4522 \times 10^{-5}$	142.1	-37.3	$0.3462 \times 10^{-5}$
17B	1	3	7	183.6	-20.9	$0.3294 \times 10^{-5}$	159.3	-23.6	$0.1905 \times 10^{-5}$
17B	1	3	50	174.7	-1.7	$0.3451 \times 10^{-5}$	140.0	-38.9	$0.7455 \times 10^{-6}$
17B	1	3	100	105.3	57.7	$0.9312 \times 10^{-6}$	176.1	-9.0	$0.1785 \times 10^{-6}$
17B	1	4	16	205.2	-0.4	$0.1302 \times 10^{-5}$	69.4	-11.2	$0.3186 \times 10^{-6}$
17B	1	4	50	194.7	10.3	$0.3463 \times 10^{-5}$	247.5	32.9	$0.8705 \times 10^{-6}$
17B	1	4	100	212.7	6.8	$0.1832 \times 10^{-5}$	238.9	20.3	$0.7531 \times 10^{-6}$
17B	1	5	32	198.9	11.2	$0.2128 \times 10^{-5}$	230.6	-15.2	$0.5601 \times 10^{-6}$
17B	1	5	50	202.4	-7.6	$0.5010 \times 10^{-5}$	220.1	-12.7	$0.2045 \times 10^{-5}$
17B	1	5	100	243.4	-26.9	$0.3211 \times 10^{-5}$	269.1	-24.8	$0.2059 \times 10^{-5}$

TABLE 1—Continued

Hole	Core	Section	Sampled at (cm)	NRM			50 oersted		
				Decl.	Incl.	Intensity emu/gm	Decl.	Incl.	Intensity emu/gm
17B	1	6	50	191.3	-17.8	—	206.5	-26.3	—
17B	1	6	100	218.2	-4.3	$0.1416 \times 10^{-5}$	321.1	-45.2	$0.5349 \times 10^{-6}$
17B	2	1	130	248.0	46.3	$0.4567 \times 10^{-5}$	311.3	50.2	$0.2880 \times 10^{-5}$
17B	2	2	14	274.0	76.6	$0.2376 \times 10^{-5}$	311.4	49.6	$0.2468 \times 10^{-5}$
17B	2	2	50	217.6	10.1	$0.3496 \times 10^{-5}$	71.5	4.5	$0.2068 \times 10^{-5}$
17B	2	2	100	171.3	14.8	$0.3801 \times 10^{-5}$	147.5	11.6	$0.2014 \times 10^{-5}$
17B	2	3	7	213.2	18.1	$0.2584 \times 10^{-5}$	257.6	21.7	$0.5978 \times 10^{-6}$
17B	2	3	50	171.8	18.7	$0.5726 \times 10^{-5}$	176.0	25.9	$0.1618 \times 10^{-5}$
17B	2	3	100	16.9	-16.2	$0.2627 \times 10^{-5}$	190.7	-41.2	$0.3786 \times 10^{-6}$
17B	2	4	16	183.5	28.6	$0.2232 \times 10^{-5}$	95.3	33.7	$0.5213 \times 10^{-6}$
17B	2	4	50	189.0	82.2	$0.1882 \times 10^{-4}$	57.0	76.0	$0.1423 \times 10^{-5}$
17B	2	4	101	164.2	19.3	$0.1899 \times 10^{-5}$	79.6	47.4	$0.5099 \times 10^{-6}$
17B	2	5	15	205.0	35.0	$0.3110 \times 10^{-5}$	277.1	58.9	$0.5819 \times 10^{-6}$
17B	2	5	50	162.9	14.0	$0.4315 \times 10^{-5}$	133.5	23.3	$0.1790 \times 10^{-5}$
17B	2	5	100	181.9	-1.9	$0.2053 \times 10^{-5}$	191.5	-31.0	$0.3972 \times 10^{-6}$
17B	2	6	7	205.7	-1.5	$0.2737 \times 10^{-5}$	241.1	32.2	$0.8526 \times 10^{-6}$
17B	2	6	66	178.1	-9.8	$0.5694 \times 10^{-5}$	175.9	-29.3	$0.2539 \times 10^{-5}$
17B	2	6	100	210.6	10.8	$0.2126 \times 10^{-5}$	280.7	13.1	$0.2921 \times 10^{-6}$
17B	3	1	17	177.8	63.3	$0.7265 \times 10^{-5}$	195.3	77.0	$0.5393 \times 10^{-5}$
17B	3	1	48	187.9	5.4	$0.5659 \times 10^{-5}$	193.2	2.5	$0.1327 \times 10^{-5}$
17B	3	1	100	148.1	40.3	$0.4993 \times 10^{-5}$	105.7	-52.3	$0.3539 \times 10^{-5}$
17B	3	2	15	198.4	-15.1	$0.1621 \times 10^{-5}$	200.1	-30.7	$0.5256 \times 10^{-6}$
17B	3	2	50	213.4	7.6	$0.3167 \times 10^{-5}$	259.5	-14.0	$0.9437 \times 10^{-6}$
17B	3	2	100	209.5	-3.6	$0.2330 \times 10^{-5}$	232.0	-6.5	$0.1237 \times 10^{-5}$
17B	3	3	17	286.4	-27.8	$0.3736 \times 10^{-5}$	314.5	-36.8	$0.3341 \times 10^{-5}$
17B	3	3	50	208.7	-20.5	$0.6050 \times 10^{-5}$	236.7	-33.6	$0.3152 \times 10^{-5}$
17B	3	3	100	196.6	30.7	$0.2576 \times 10^{-5}$	247.5	-30.1	$0.8672 \times 10^{-6}$
17B	3	4	16	200.4	-29.2	$0.2337 \times 10^{-5}$	188.1	-77.3	$0.9181 \times 10^{-6}$
17B	3	4	50	178.0	1.7	$0.2398 \times 10^{-5}$	209.9	-14.7	$0.8352 \times 10^{-6}$

TABLE 1—Continued

Hole	Core	Section	Sampled at (cm)	NRM			50 oersted		
				Decl.	Incl.	Intensity emu/gm	Decl.	Incl.	Intensity emu/gm
17B	3	4	100	194.8	11.8	$0.3238 \times 10^{-5}$	202.6	-21.0	$0.1493 \times 10^{-5}$
17B	3	5	27	205.2	-32.7	$0.6053 \times 10^{-5}$	219.5	-20.3	$0.7549 \times 10^{-6}$
17B	3	5	101	201.3	13.3	$0.3590 \times 10^{-5}$	199.6	2.8	$0.1024 \times 10^{-5}$
17B	3	6	25	154.1	-22.2	$0.5830 \times 10^{-5}$	152.9	-25.2	$0.4475 \times 10^{-5}$
17B	3	6	46	232.6	-39.3	$0.4687 \times 10^{-5}$	268.1	-44.2	$0.3178 \times 10^{-5}$
17B	3	6	100	198.8	-40.3	$0.1907 \times 10^{-5}$	198.3	-73.9	$0.9210 \times 10^{-6}$
17B	4	1	34	239.7	-47.1	$0.6223 \times 10^{-5}$	252.2	-48.7	$0.4452 \times 10^{-5}$
17B	4	1	50	224.3	-20.9	$0.8302 \times 10^{-5}$	239.2	-22.9	$0.4970 \times 10^{-5}$
17B	4	1	100	229.5	-13.6	$0.2864 \times 10^{-5}$	244.6	-25.9	$0.1593 \times 10^{-5}$
17B	4	2	6	220.5	-6.4	$0.4860 \times 10^{-5}$	233.1	-15.5	$0.3312 \times 10^{-5}$
17B	4	2	50	222.8	-12.7	$0.5691 \times 10^{-5}$	250.5	-20.1	$0.3014 \times 10^{-5}$
17B	4	2	102	183.0	17.5	$0.1033 \times 10^{-5}$	46.2	-43.3	$0.2578 \times 10^{-6}$
17B	4	3	2	64.9	-20.2	$0.2301 \times 10^{-5}$	45.5	-26.8	$0.2818 \times 10^{-5}$
17B	4	3	51	173.3	-18.8	$0.6303 \times 10^{-5}$	167.4	-49.5	$0.2287 \times 10^{-5}$
17B	4	3	100	172.5	23.6	$0.9821 \times 10^{-6}$	55.7	3.0	$0.3681 \times 10^{-6}$
17B	4	4	15	155.6	15.7	$0.2889 \times 10^{-5}$	127.0	7.0	$0.1998 \times 10^{-5}$
17B	4	4	50	175.3	-13.3	$0.3543 \times 10^{-5}$	170.6	-32.9	$0.1309 \times 10^{-5}$
17B	4	4	102	255.2	31.3	$0.1871 \times 10^{-5}$	311.8	28.1	$0.1029 \times 10^{-5}$
17B	4	5	4	201.4	7.4	$0.1721 \times 10^{-5}$	204.8	11.5	$0.5866 \times 10^{-6}$
17B	4	5	50	187.6	-5.8	$0.4655 \times 10^{-5}$	188.7	-5.6	$0.1858 \times 10^{-5}$
17B	4	5	100	245.0	7.6	$0.2271 \times 10^{-5}$	268.6	7.8	$0.1573 \times 10^{-5}$
17B	4	6	3	172.9	-14.6	$0.1986 \times 10^{-5}$	94.6	-58.7	$0.7147 \times 10^{-6}$
*17B	4	6	53.5	119.0	37.3	$0.3782 \times 10^{-5}$	88.9	30.9	$0.2551 \times 10^{-5}$
17B	4	6	101	208.7	-35.2	$0.3118 \times 10^{-5}$	255.1	-6.3	$0.1297 \times 10^{-5}$
18	2	2	3	42.7	-67.3	$0.6812 \times 10^{-5}$	50.5	-58.6	$0.5715 \times 10^{-5}$
18	2	2	100	276.9	-65.8	$0.4287 \times 10^{-5}$	352.3	-71.9	$0.3785 \times 10^{-5}$
18	3	2	2	341.8	-69.1	$0.2644 \times 10^{-5}$	191.1	-59.5	$0.2323 \times 10^{-5}$
18	3	2	103	63.4	-88.9	$0.5220 \times 10^{-5}$	—	—	—
18	4	4	6	121.8	-62.4	$0.2995 \times 10^{-5}$	104.7	-52.8	$0.1999 \times 10^{-5}$

TABLE 1—Continued

Hole	Core	Section	Sampled at (cm)	NRM			50 oersted		
				Decl.	Incl.	Intensity emu/gm	Decl.	Incl.	Intensity emu/gm
18	4	4	50	156.5	-45.1	$0.3213 \times 10^{-5}$	98.6	-87.3	$0.1298 \times 10^{-4}$
18	4	4	100	77.5	-56.5	$0.2303 \times 10^{-5}$	58.5	-60.8	$0.1523 \times 10^{-5}$
18	5	2	7	203.9	17.7	$0.9159 \times 10^{-6}$	224.4	-35.5	$0.6934 \times 10^{-6}$
18	5	2	48	197.0	7.3	$0.2480 \times 10^{-5}$	174.0	13.0	$0.6605 \times 10^{-6}$
18	5	2	127	195.4	29.5	$0.2068 \times 10^{-5}$	188.8	35.3	$0.5866 \times 10^{-6}$
18	6	1	15	106.6	38.0	$0.2945 \times 10^{-5}$	86.3	44.9	$0.2667 \times 10^{-5}$
18	6	1	100	193.1	-2.2	$0.2211 \times 10^{-5}$	205.6	18.5	$0.1014 \times 10^{-5}$
18	6	6	5	140.0	34.4	$0.1946 \times 10^{-5}$	84.4	64.6	$0.9542 \times 10^{-6}$
18	6	6	50	177.0	33.7	$0.3812 \times 10^{-5}$	216.9	61.9	$0.1903 \times 10^{-5}$
*18	6	6	75-7	162.0	43.7	$0.1382 \times 10^{-5}$	146.4	77.0	$0.1198 \times 10^{-5}$
18	6	6	100	233.1	36.6	$0.2427 \times 10^{-5}$	249.5	47.3	$0.1665 \times 10^{-5}$
*19	1	2	2-4	196.3	2.9	$0.7059 \times 10^{-5}$	250.6	48.8	$0.2677 \times 10^{-5}$
19	3	1	50	225.7	-65.4	$0.7663 \times 10^{-5}$	223.2	-76.9	$0.6776 \times 10^{-5}$
19	3	1	105	155.7	-50.9	$0.9160 \times 10^{-5}$	99.8	-56.1	$0.4461 \times 10^{-5}$
19	3	2	14	206.2	39.1	$0.5107 \times 10^{-5}$	223.2	35.4	$0.2561 \times 10^{-5}$
19	3	2	50	199.6	-15.8	$0.1860 \times 10^{-4}$	207.2	-37.8	$0.9891 \times 10^{-5}$
19	3	2	100	233.6	-45.6	$0.1666 \times 10^{-4}$	100.7	-66.4	$0.8179 \times 10^{-5}$
19	3	3	13	184.5	43.3	$0.8833 \times 10^{-5}$	110.1	44.7	$0.1375 \times 10^{-5}$
19	3	3	100	208.1	24.8	$0.8000 \times 10^{-5}$	302.8	34.6	$0.1827 \times 10^{-5}$
19	3	4	13	172.2	8.2	$0.1421 \times 10^{-4}$	169.8	-6.2	$0.4907 \times 10^{-5}$
19	3	4	100	107.4	-58.5	$0.8841 \times 10^{-5}$	41.0	-57.0	$0.6281 \times 10^{-5}$
19	3	5	10	121.1	-19.7	$0.7936 \times 10^{-5}$	87.2	-46.0	$0.5576 \times 10^{-5}$
19	3	5	130	208.0	9.2	$0.6194 \times 10^{-5}$	344.9	46.9	$0.2788 \times 10^{-5}$
19	3	6	12	148.2	19.4	$0.9194 \times 10^{-5}$	85.4	56.0	$0.3398 \times 10^{-5}$
19	3	6	105	183.3	19.3	$0.6052 \times 10^{-5}$	236.4	28.4	$0.1045 \times 10^{-5}$
19	3	6	130	230.6	35.2	$0.7140 \times 10^{-5}$	294.9	12.7	$0.2638 \times 10^{-5}$
19	4	2	1	311.2	-28.7	$0.2007 \times 10^{-4}$	319.1	-21.3	$0.1819 \times 10^{-4}$
19	4	2	23	219.2	51.7	$0.5802 \times 10^{-5}$	218.4	63.5	$0.3877 \times 10^{-5}$
19	4	2	100	129.7	-10.6	$0.1592 \times 10^{-4}$	125.5	-15.6	$0.1190 \times 10^{-4}$

TABLE 1—Continued

Hole	Core	Section	Sampled at (cm)	NRM			50 oersted		
				Decl.	Incl.	Intensity emu/gm	Decl.	Incl.	Intensity emu/gm
19	5	2	1	189.0	-47.2	$0.4409 \times 10^{-5}$	161.5	-80.1	$0.8539 \times 10^{-6}$
19	5	2	13	175.9	3.5	$0.4569 \times 10^{-5}$	168.0	-12.4	$0.1607 \times 10^{-5}$
19	5	2	50	173.1	34.7	$0.1183 \times 10^{-4}$	155.7	37.2	$0.8153 \times 10^{-5}$
19	5	2	100	202.8	52.1	$0.4586 \times 10^{-5}$	213.6	55.9	$0.3957 \times 10^{-5}$
19	5	3	3	169.3	34.9	$0.1812 \times 10^{-4}$	151.1	37.8	$0.1106 \times 10^{-5}$
19	5	3	8	127.8	71.2	$0.6653 \times 10^{-5}$	67.6	53.2	$0.6310 \times 10^{-5}$
19	5	3	51	153.7	20.0	$0.1484 \times 10^{-4}$	138.3	33.2	$0.9011 \times 10^{-5}$
19	5	3	100	183.9	61.0	$0.5072 \times 10^{-5}$	82.7	66.0	$0.3570 \times 10^{-5}$
19	5	4	19	195.2	-78.5	$0.5469 \times 10^{-5}$	80.9	-74.5	$0.3639 \times 10^{-5}$
19	5	4	50	194.9	-6.7	$0.1022 \times 10^{-4}$	192.7	-12.2	$0.4276 \times 10^{-5}$
19	5	4	100	133.9	-33.4	$0.8778 \times 10^{-5}$	119.6	-49.2	$0.5503 \times 10^{-5}$
19	5	5	12	31.3	-73.6	$0.6553 \times 10^{-5}$	24.1	-65.2	$0.5193 \times 10^{-5}$
19	5	5	50	218.9	-20.1	$0.9402 \times 10^{-5}$	241.1	-48.8	$0.5962 \times 10^{-5}$
19	5	5	100	140.8	30.9	$0.6848 \times 10^{-5}$	226.7	44.3	$0.4959 \times 10^{-5}$
19	5	6	3	194.6	-43.0	$0.1030 \times 10^{-4}$	115.3	-72.2	$0.3381 \times 10^{-5}$
19	5	6	10	278.9	-45.9	$0.6605 \times 10^{-5}$	310.1	-43.6	$0.3487 \times 10^{-5}$
19	5	6	50	207.4	45.9	$0.8984 \times 10^{-5}$	286.1	62.3	$0.4301 \times 10^{-5}$
19	5	6	100	163.9	60.4	$0.5249 \times 10^{-5}$	146.7	76.4	$0.3023 \times 10^{-5}$
19	7	1	10	214.8	30.2	$0.9405 \times 10^{-5}$	175.8	71.3	$0.6385 \times 10^{-5}$
19	7	1	50	175.1	-1.4	$0.9867 \times 10^{-5}$	146.6	40.2	$0.2912 \times 10^{-5}$
19	7	1	100	203.4	27.7	$0.5969 \times 10^{-5}$	228.7	50.7	$0.3701 \times 10^{-5}$
19	7	2	11	213.6	-38.0	$0.8690 \times 10^{-5}$	220.1	-31.0	$0.3788 \times 10^{-5}$
19	7	2	50	157.8	-14.4	$0.1328 \times 10^{-4}$	144.0	-25.6	$0.8802 \times 10^{-5}$
19	7	2	100	120.2	-57.8	$0.5563 \times 10^{-5}$	93.6	-61.0	$0.3912 \times 10^{-5}$
19	7	3	2	265.1	-35.2	$0.9947 \times 10^{-5}$	296.8	-41.7	$0.7003 \times 10^{-5}$
19	7	3	11	156.8	-40.5	$0.8824 \times 10^{-5}$	143.6	-51.3	$0.4962 \times 10^{-5}$
19	7	3	100	80.5	-36.4	$0.1111 \times 10^{-4}$	67.0	-35.7	$0.8601 \times 10^{-5}$
19	7	4	4	171.6	35.5	$0.1524 \times 10^{-4}$	255.5	-18.3	$0.3098 \times 10^{-5}$
19	7	4	50	193.8	35.9	$0.1104 \times 10^{-4}$	340.0	60.8	$0.4950 \times 10^{-5}$

TABLE 1—Continued

Hole	Core	Section	Sampled at (cm)	NRM			50 oersted		
				Decl.	Incl.	Intensity emu/gm	Decl.	Incl.	Intensity emu/gm
19	7	4	100	234.5	21.7	$0.6918 \times 10^{-5}$	264.4	40.8	$0.4588 \times 10^{-5}$
19	7	5	3	219.4	-18.1	$0.1040 \times 10^{-4}$	348.5	-74.2	$0.2501 \times 10^{-5}$
19	7	5	9	220.7	-48.6	$0.1142 \times 10^{-4}$	244.6	-56.4	$0.5188 \times 10^{-5}$
19	7	5	100	197.1	36.8	$0.2898 \times 10^{-5}$	22.3	33.8	$0.1765 \times 10^{-5}$
19	7	6	3	199.8	-43.0	$0.1225 \times 10^{-4}$	121.3	36.2	$0.1928 \times 10^{-5}$
19	7	6	11	171.0	15.3	$0.4810 \times 10^{-5}$	152.0	62.2	$0.3323 \times 10^{-5}$
19	7	6	50	151.9	8.3	$0.3286 \times 10^{-5}$	119.5	-18.3	$0.3119 \times 10^{-6}$
19	7	6	62	238.7	-24.3	$0.1063 \times 10^{-5}$	284.8	60.2	$0.3773 \times 10^{-6}$
19	8	2	11	64.1	44.9	$0.4631 \times 10^{-5}$	62.2	30.7	$0.2102 \times 10^{-5}$
19	8	2	46	221.7	-10.9	$0.7781 \times 10^{-5}$	225.0	-26.5	$0.4849 \times 10^{-5}$
19	8	2	102	273.0	-46.8	$0.4872 \times 10^{-5}$	287.2	-33.3	$0.5513 \times 10^{-5}$
19	9	6	12	146.5	-37.5	$0.5664 \times 10^{-5}$	156.2	-72.2	$0.9282 \times 10^{-5}$
19	9	6	50	209.1	-19.0	$0.1280 \times 10^{-4}$	219.1	-33.8	$0.4417 \times 10^{-5}$
19	9	6	70	317.0	-33.9	$0.7935 \times 10^{-5}$	338.1	-35.6	$0.3454 \times 10^{-5}$
20A	2	1	54	210.9	-64.5	$0.4891 \times 10^{-5}$	270.4	-25.7	$0.7967 \times 10^{-5}$
20A	2	1	100	167.9	-11.4	$0.5863 \times 10^{-5}$	169.9	2.0	$0.2897 \times 10^{-5}$
20A	2	2	13	155.9	-78.7	$0.1488 \times 10^{-5}$	112.4	-11.5	$0.2910 \times 10^{-5}$
*20A	2	2	50-2	216.3	-14.0	$0.1419 \times 10^{-5}$	295.9	22.7	$0.4284 \times 10^{-6}$
20A	2	2	120	219.9	2.2	$0.3711 \times 10^{-5}$	201.8	72.3	$0.1332 \times 10^{-5}$
20A	2	3	14	168.0	17.5	$0.2752 \times 10^{-5}$	43.9	71.4	$0.2304 \times 10^{-5}$
20B	1	1	10	113.7	-47.2	$0.7503 \times 10^{-5}$	293.3	-29.1	$0.5105 \times 10^{-5}$
20B	1	1	50	165.6	-10.3	$0.2130 \times 10^{-4}$	147.9	8.3	$0.3827 \times 10^{-5}$
*20B	1	2	7-9	207.1	-16.7	$0.7617 \times 10^{-5}$	281.9	-40.6	$0.4168 \times 10^{-5}$
20B	1	2	14	179.5	6.8	$0.4395 \times 10^{-5}$	303.5	-39.8	$0.1424 \times 10^{-5}$
20B	1	2	50	200.4	9.1	$0.2240 \times 10^{-4}$	211.2	-28.8	$0.5591 \times 10^{-5}$
20B	1	2	102	150.0	-0.4	$0.9467 \times 10^{-5}$	174.2	11.6	$0.1425 \times 10^{-5}$
20B	1	3	4	165.7	12.9	$0.2239 \times 10^{-4}$	129.4	-32.4	$0.2128 \times 10^{-5}$
20B	1	3	12	184.4	-39.2	$0.5292 \times 10^{-5}$	113.2	48.4	$0.1001 \times 10^{-5}$
20B	1	3	50	189.3	3.0	$0.1793 \times 10^{-4}$	185.3	-34.7	$0.3701 \times 10^{-5}$

TABLE 1—Continued

Hole	Core	Section	Sampled at (cm)	NRM			50 oersted		
				Decl.	Incl.	Intensity emu/gm	Decl.	Incl.	Intensity emu/gm
20B	1	3	100	163.3	-30.6	$0.8165 \times 10^{-5}$	149.1	-45.2	$0.2864 \times 10^{-5}$
20B	1	4	3	207.1	-2.8	$0.2106 \times 10^{-4}$	112.3	-75.2	$0.4515 \times 10^{-5}$
20B	1	4	13	150.6	-47.1	$0.9214 \times 10^{-5}$	112.1	-69.2	$0.3432 \times 10^{-5}$
20B	1	4	100	216.6	-14.7	$0.9180 \times 10^{-5}$	111.9	-81.2	$0.3831 \times 10^{-5}$
20B	1	5	0-2	183.0	-36.6	$0.2722 \times 10^{-4}$	132.1	-71.0	$0.3987 \times 10^{-5}$
20B	1	5	50	185.3	-20.4	$0.1927 \times 10^{-4}$	324.9	-55.8	$0.6127 \times 10^{-5}$
20B	1	5	110	177.5	-17.6	$0.6843 \times 10^{-5}$	50.9	-50.4	$0.5974 \times 10^{-6}$
20B	1	6	1	205.7	-2.3	$0.2732 \times 10^{-4}$	182.6	-39.0	$0.3327 \times 10^{-5}$
20B	1	6	100	256.9	-35.2	$0.1017 \times 10^{-4}$	266.4	-2.5	$0.6197 \times 10^{-5}$
20C	1	1	50	178.7	-24.0	$0.2347 \times 10^{-4}$	185.8	-39.6	$0.1039 \times 10^{-4}$
20C	1	1	60	179.4	27.2	$0.6251 \times 10^{-5}$	170.4	53.4	$0.5701 \times 10^{-5}$
20C	1	2	146	306.8	41.2	$0.3867 \times 10^{-5}$	353.2	40.8	$0.6109 \times 10^{-5}$
20C	1	3	68	247.6	14.4	$0.1542 \times 10^{-4}$	284.4	23.4	$0.1070 \times 10^{-4}$
20C	1	3	76	234.0	26.8	$0.1720 \times 10^{-4}$	116.8	31.4	$0.1478 \times 10^{-4}$
20C	1	5	3	105.6	12.3	$0.7800 \times 10^{-5}$	68.5	32.9	$0.7332 \times 10^{-5}$
20C	1	5	105	200.9	-41.4	$0.1179 \times 10^{-4}$	198.6	-66.0	$0.6036 \times 10^{-5}$
20C	1	6	22	174.5	0.9	$0.2537 \times 10^{-4}$	178.3	3.2	$0.1067 \times 10^{-4}$
20C	1	6	50	142.1	-46.5	$0.1387 \times 10^{-4}$	85.1	-48.9	$0.8655 \times 10^{-5}$
20C	1	6	99	181.3	-5.5	$0.7148 \times 10^{-5}$	147.4	-50.6	$0.1273 \times 10^{-5}$
20C	2	3	68	204.9	-4.9	$0.4258 \times 10^{-5}$	198.9	8.9	$0.2716 \times 10^{-5}$
20C	2	4	12	223.1	-4.3	$0.2159 \times 10^{-5}$	264.2	6.2	$0.1464 \times 10^{-5}$
20C	2	4	50	148.6	-5.2	$0.2132 \times 10^{-5}$	327.1	-25.2	$0.5972 \times 10^{-6}$
20C	2	4	112	222.1	20.0	$0.1459 \times 10^{-5}$	269.5	15.5	$0.6307 \times 10^{-6}$
20C	3	1	13	166.6	30.5	$0.8725 \times 10^{-5}$	161.4	25.8	$0.8435 \times 10^{-5}$
20C	3	1	50	169.2	-29.2	$0.4055 \times 10^{-4}$	202.4	-26.2	$0.5790 \times 10^{-5}$
20C	3	3	19	188.2	20.9	$0.9178 \times 10^{-5}$	87.0	59.1	$0.3621 \times 10^{-5}$
20C	3	4	22	211.1	-43.4	$0.6558 \times 10^{-5}$	3.2	-50.1	$0.1771 \times 10^{-5}$
20C	3	4	38	193.2	-19.8	$0.2625 \times 10^{-4}$	245.8	-35.4	$0.7304 \times 10^{-5}$
20C	3	4	77	197.0	15.3	$0.9409 \times 10^{-5}$	199.8	33.1	$0.2800 \times 10^{-5}$

TABLE 1—Continued

Hole	Core	Section	Sampled at (cm)	NRM			50 oersted		
				Decl.	Incl.	Intensity emu/gm	Decl.	Incl.	Intensity emu/gm
20C	3	5	62	211.3	32.0	$0.6928 \times 10^{-5}$	218.3	18.0	$0.6473 \times 10^{-5}$
20C	3	5	122	176.2	-75.7	$0.9665 \times 10^{-5}$	351.3	-80.6	$0.5684 \times 10^{-5}$
20C	3	6	17	202.8	65.2	$0.1108 \times 10^{-4}$	325.3	18.5	$0.3406 \times 10^{-5}$
20C	3	6	104	168.2	20.8	$0.7547 \times 10^{-5}$	221.4	41.3	$0.2823 \times 10^{-5}$
20C	4	2	21	167.0	69.9	$0.1637 \times 10^{-4}$	132.8	56.0	$0.7224 \times 10^{-5}$
20C	4	3	9	252.6	8.2	$0.2629 \times 10^{-4}$	263.6	2.3	$0.3236 \times 10^{-4}$
20C	4	3	100	287.8	-18.3	$0.1174 \times 10^{-3}$	250.3	-17.2	$0.1131 \times 10^{-3}$
20C	5	2	13	277.0	3.2	$0.1387 \times 10^{-3}$	259.5	4.6	$0.1300 \times 10^{-3}$
20C	5	4	8	246.2	3.3	$0.5265 \times 10^{-5}$	269.1	-11.0	$0.3200 \times 10^{-5}$
*20C	5	4	60-62	166.7	1.5	$0.3578 \times 10^{-5}$	148.2	30.7	$0.6745 \times 10^{-6}$
20C	5	4	100	355.3	2.2	$0.3080 \times 10^{-5}$	216.4	30.9	$0.5961 \times 10^{-6}$
20C	5	5	14	170.8	20.1	$0.6394 \times 10^{-5}$	175.8	-26.3	$0.7696 \times 10^{-6}$
20C	5	5	50	178.6	-13.1	$0.7392 \times 10^{-5}$	185.6	-15.9	$0.5493 \times 10^{-6}$
20C	5	5	105	181.9	18.4	$0.2392 \times 10^{-5}$	101.2	65.6	$0.6194 \times 10^{-6}$
20C	5	6	11	170.1	-6.1	$0.2102 \times 10^{-5}$	148.7	25.4	$0.5192 \times 10^{-6}$
20C	5	6	100	144.3	-51.5	$0.4119 \times 10^{-5}$	132.5	-27.3	$0.4498 \times 10^{-6}$
20C	6	4	2	192.8	-4.2	$0.8174 \times 10^{-5}$	63.1	73.1	$0.1112 \times 10^{-5}$
20C	6	4	5	179.1	5.8	$0.2250 \times 10^{-5}$	139.6	55.2	$0.1295 \times 10^{-5}$
20C	6	4	85	190.5	-10.8	—	262.4	56.3	—
20C	6	4	100	204.9	-10.5	$0.4681 \times 10^{-5}$	334.4	26.2	$0.1095 \times 10^{-5}$
20C	6	4	112	62.1	-17.6	$0.5592 \times 10^{-5}$	39.8	-17.4	$0.5014 \times 10^{-5}$
20C	6	4	134	192.9	11.7	$0.5597 \times 10^{-5}$	144.4	25.1	$0.9621 \times 10^{-6}$
20C	6	5	0-2	162.1	-30.3	$0.6371 \times 10^{-5}$	242.2	-37.2	$0.6302 \times 10^{-6}$
20C	6	5	8	182.3	6.9	$0.6048 \times 10^{-5}$	333.6	40.9	$0.4160 \times 10^{-6}$
20C	6	5	19	228.9	21.4	$0.2693 \times 10^{-5}$	292.6	22.3	$0.1135 \times 01^{-5}$
20C	6	5	30	288.2	53.9	$0.5554 \times 10^{-5}$	319.4	44.3	$0.4363 \times 10^{-5}$
20C	6	5	40	161.5	51.8	$0.6914 \times 10^{-5}$	145.3	59.2	$0.3261 \times 10^{-5}$
20C	6	5	75	343.2	77.3	$0.1164 \times 10^{-4}$	3.2	71.3	$0.9614 \times 10^{-5}$
20C	6	5	78	200.1	64.4	$0.1719 \times 10^{-4}$	289.0	77.3	$0.1261 \times 10^{-4}$

TABLE I—Continued

Hole	Core	Section	Sampled at (cm)	NRM			50 oersted		
				Decl.	Incl.	Intensity emu/gm	Decl.	Incl.	Intensity emu/gm
20C	6	5	100	138.0	72.4	$0.1094 \times 10^{-4}$	130.1	86.0	$0.7779 \times 10^{-5}$
20C	6	5	140	195.4	-25.5	$0.7973 \times 10^{-5}$	288.3	-51.4	$0.3462 \times 10^{-5}$
21	2	6	143	194.4	34.4	$0.6114 \times 10^{-5}$	327.2	40.3	$0.1835 \times 10^{-5}$
21	6	3	7	186.0	-3.9	$0.6767 \times 10^{-5}$	217.9	-51.9	$0.2017 \times 10^{-5}$
21	6	4	2	142.9	-34.7	$0.7828 \times 10^{-5}$	101.8	-50.2	$0.2321 \times 10^{-5}$
21	6	4	100	205.9	-43.9	$0.3435 \times 10^{-5}$	261.3	-53.4	$0.1881 \times 10^{-5}$
21	6	5	3	163.5	-19.7	$0.9373 \times 10^{-5}$	152.7	-46.6	$0.5062 \times 10^{-5}$
21	6	5	100	293.7	-47.7	$0.7274 \times 10^{-5}$	283.9	-18.3	$0.3287 \times 10^{-5}$
*21	6	6	3-5	156.7	41.9	$0.9655 \times 10^{-5}$	147.8	45.5	$0.6133 \times 10^{-5}$
21	6	6	100	241.0	-50.6	$0.2291 \times 10^{-5}$	241.0	-59.9	$0.1756 \times 10^{-5}$
21A	3	6	20	165.5	28.4	$0.3620 \times 10^{-5}$	149.5	37.6	$0.1851 \times 10^{-5}$
21A	3	6	80	187.2	21.6	$0.2759 \times 10^{-5}$	131.1	22.1	$0.1308 \times 10^{-5}$
21A	3	6	136	233.9	53.8	$0.4372 \times 10^{-5}$	45.0	70.3	$0.2370 \times 10^{-5}$
22	1	6	60	218.9	-14.1	$0.2548 \times 10^{-5}$	235.3	-26.3	$0.1500 \times 10^{-5}$
22	1	6	100	182.8	-69.9	$0.3759 \times 10^{-6}$	199.1	-73.8	$0.2808 \times 10^{-6}$
22	4	2	55	254.3	16.4	$0.2302 \times 10^{-6}$	242.2	19.6	$0.2735 \times 10^{-6}$
22	4	4	100	332.7	-77.9	$0.3570 \times 10^{-6}$	338.4	-74.5	$0.3757 \times 10^{-6}$
22	4	5	100	133.8	-35.5	$0.1430 \times 10^{-5}$	130.3	-35.7	$0.1234 \times 10^{-5}$
22	4	6	13	35.2	-69.3	$0.3452 \times 10^{-6}$	62.0	-77.8	$0.3583 \times 10^{-6}$

*Figures 1-13*

Alternating field demagnetization curves for pilot specimens from Sites 13 through 21.

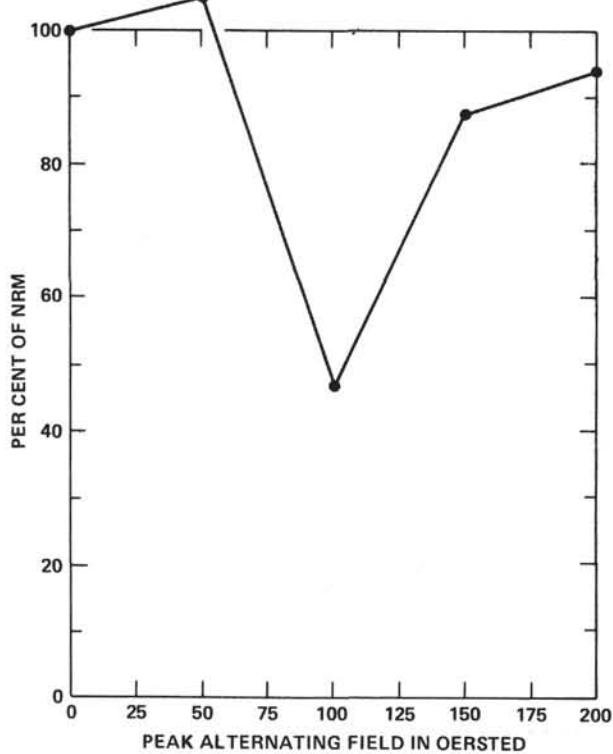


Figure 1. 3-13A-5-1, depth 49-51 cm.

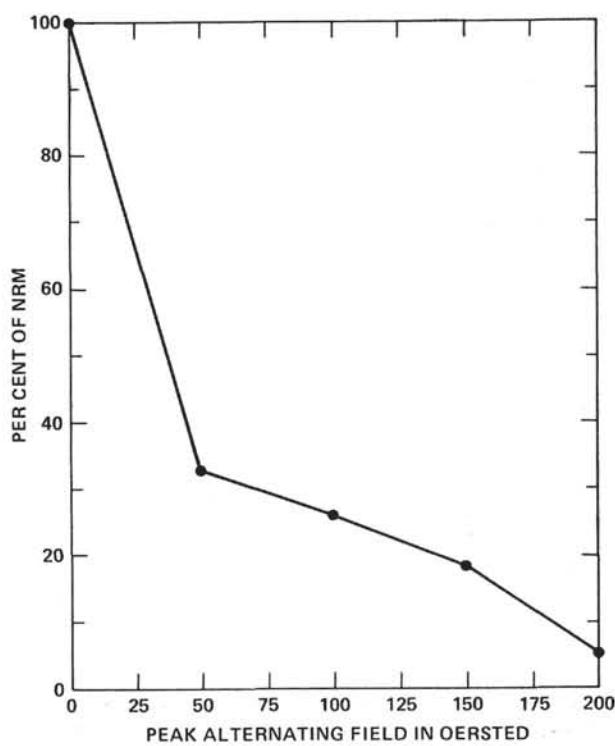


Figure 2. 3-14A-1-3, depth 50-52 cm.

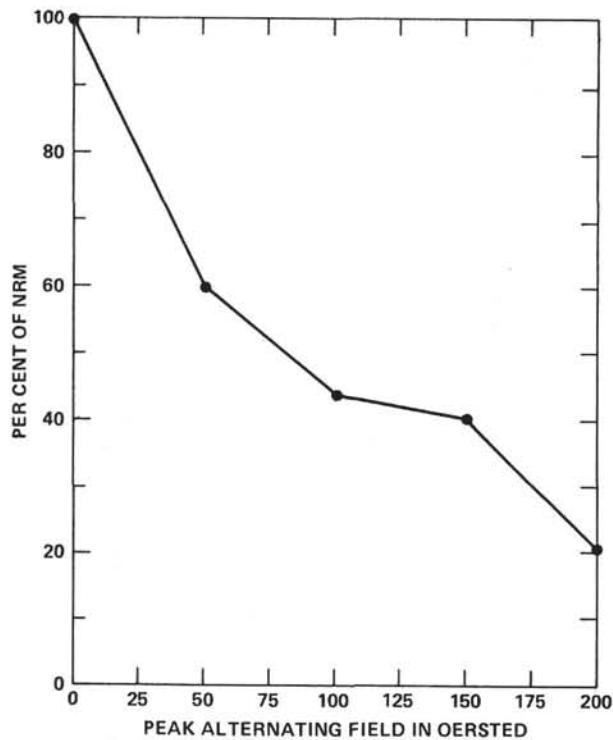


Figure 3. 3-15-4-3, depth 41-43 cm.

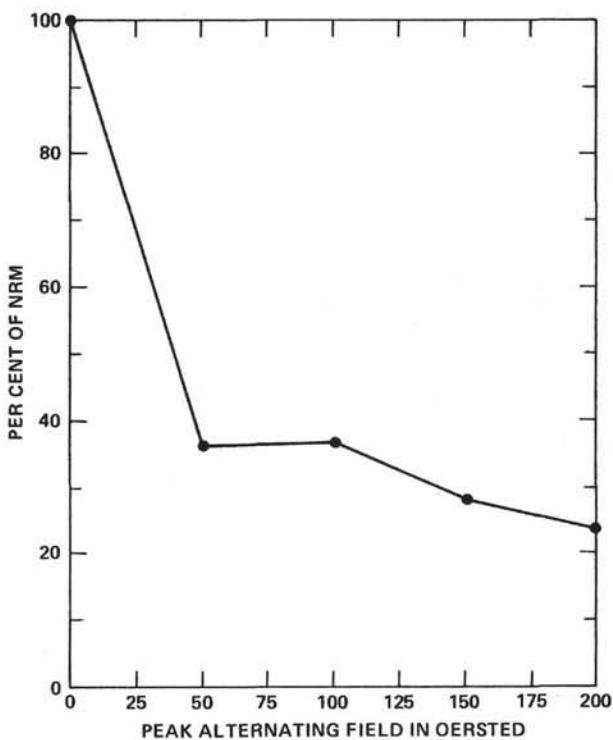


Figure 4. 3-16-2-6, depth 50-52 cm.

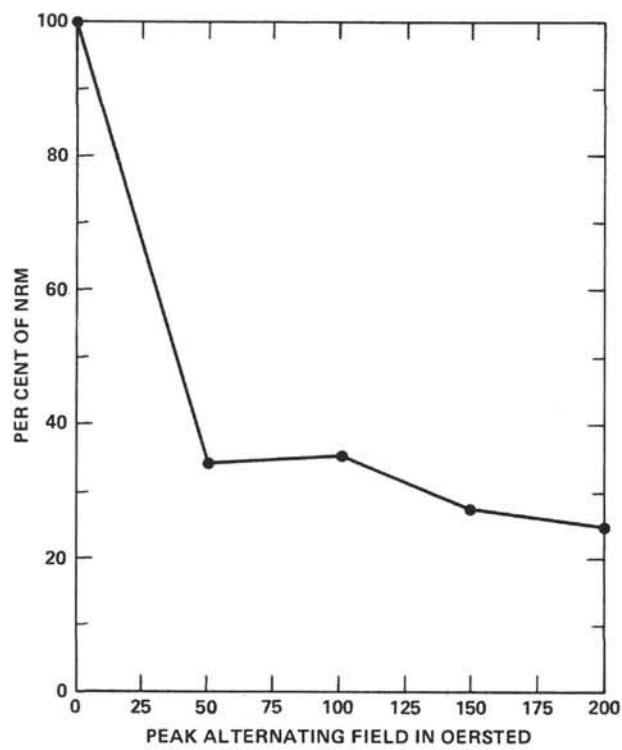


Figure 5. 3-17-2-3, depth 54-56 cm.

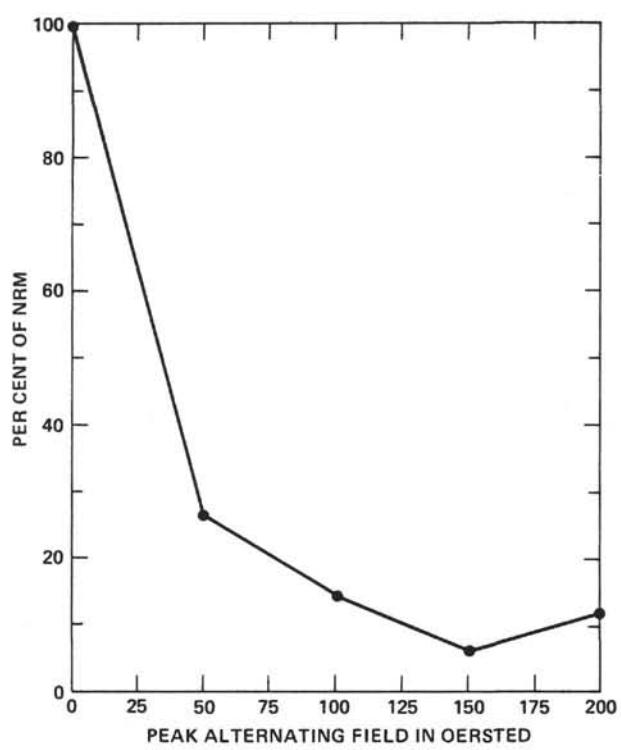


Figure 6. 3-17A-2-4, depth 50-52 cm.

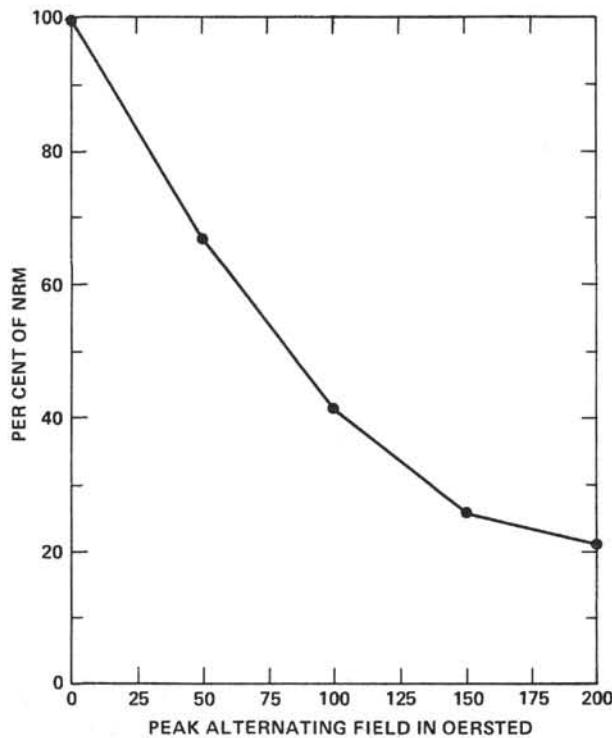


Figure 7. 3-17B-4-6, depth 53-55 cm.

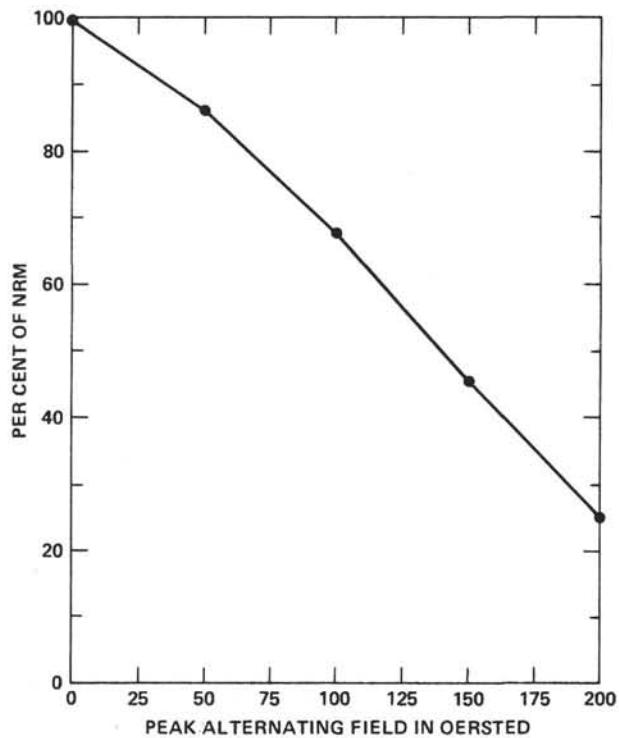


Figure 8. 3-18-6-6, depth 75-77 cm.

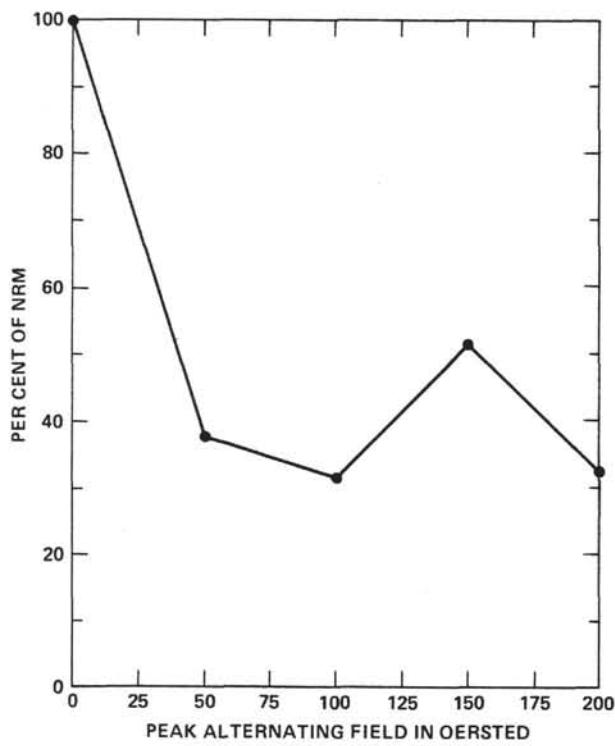


Figure 9. 3-19-I-2, depth 2-4 cm.

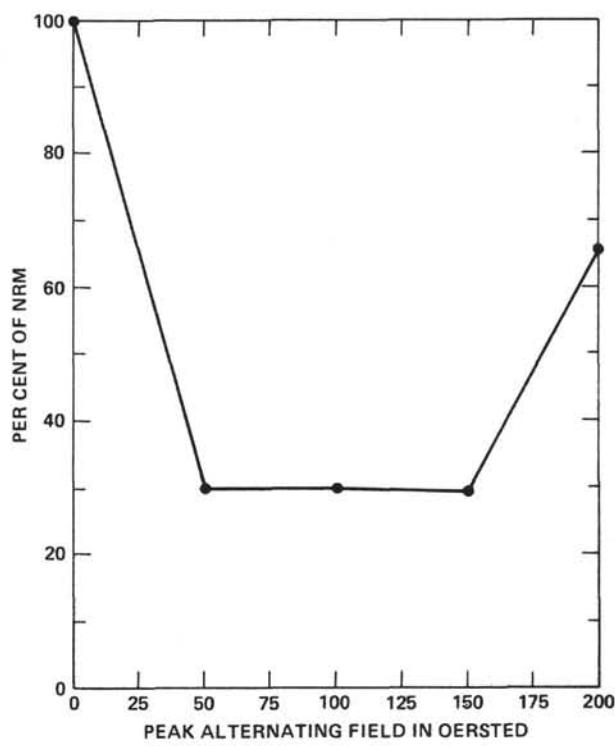


Figure 10. 3-20A-2-2, depth 50-52 cm.

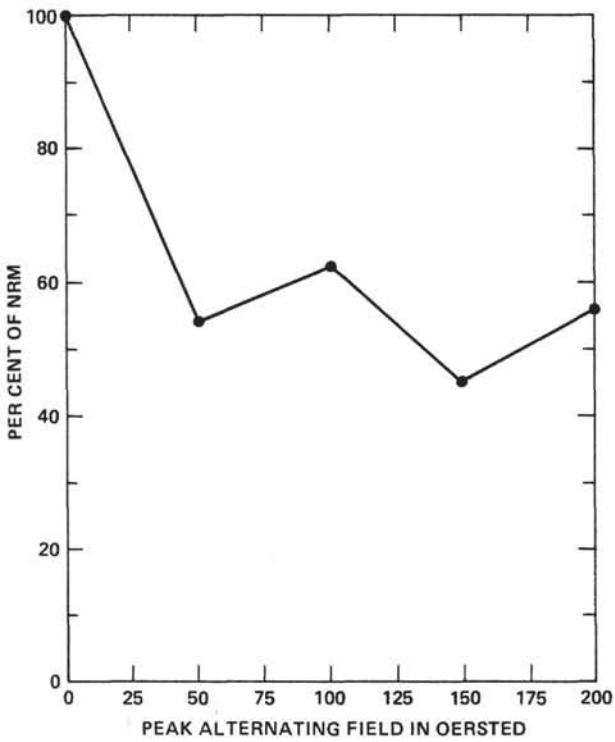


Figure 11. 3-20B-1-2, depth 7-9 cm.

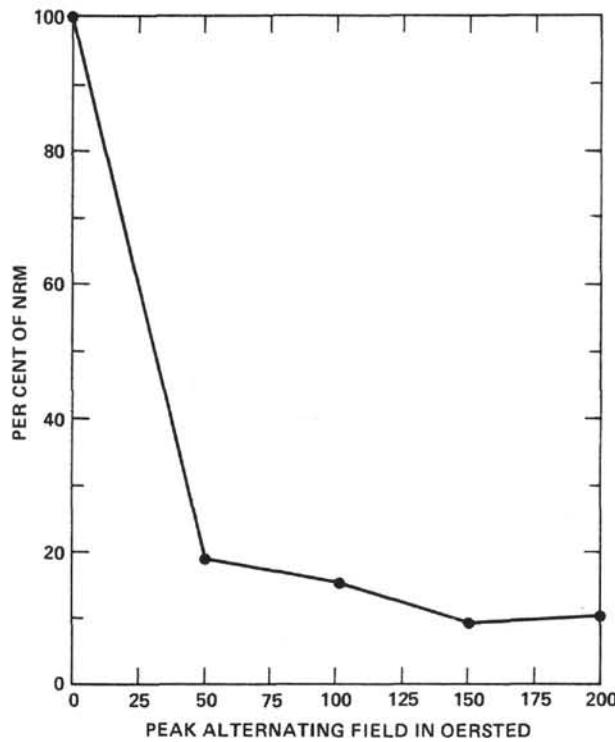


Figure 12. 3-20C-5-4, depth 60-62 cm.

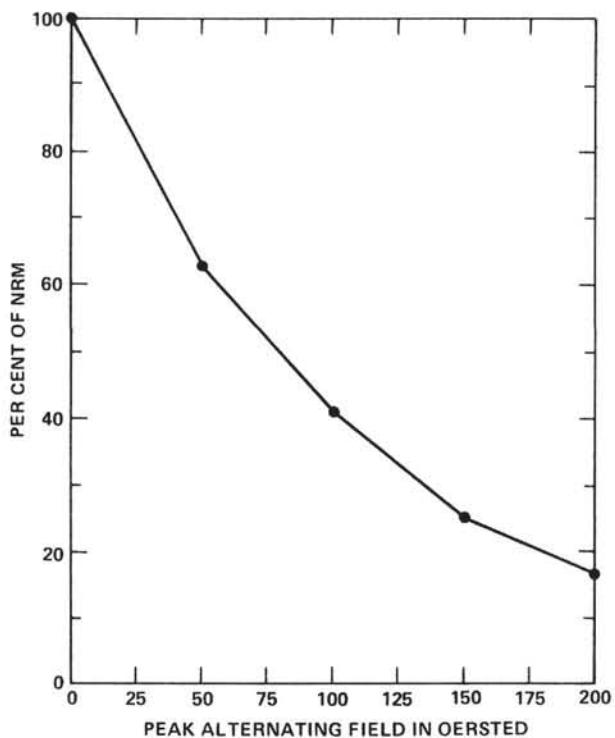


Figure 13. 3-21-6-6, depth 3.5 cm.

Figures 14 through 20

*Magnetic Stratigraphies of Sites 14 through 20*

Normal field direction is indicated in black; reversed field is striped. Actual sampled points are indicated by arrows. A scale of depth below the ocean floor in meters is shown at the left; ages are indicated to the right. All polarities are based on measurement after A-F demagnetization in 50 oersteds.

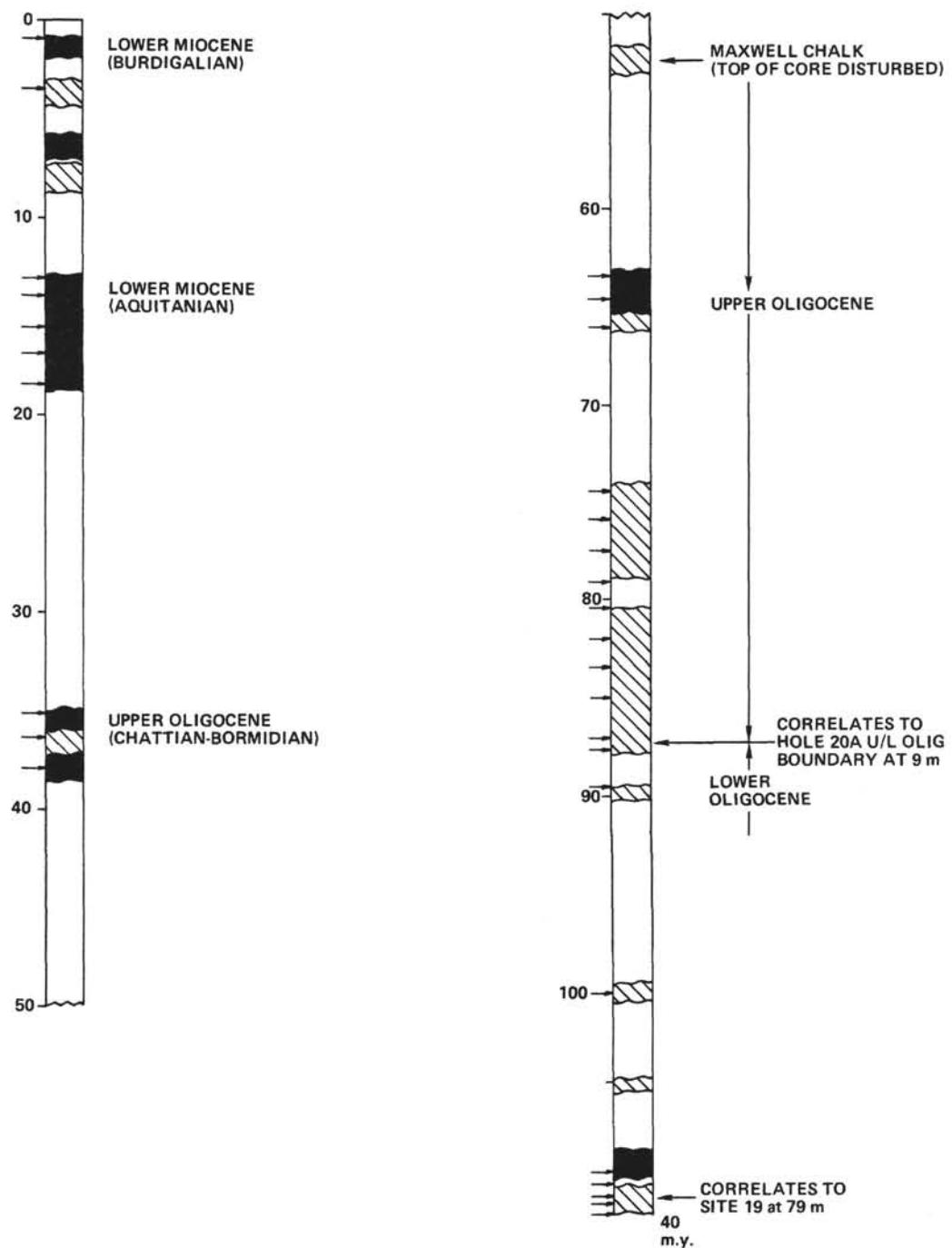


Figure 14. *Magnetic Stratigraphy of Site 14.*

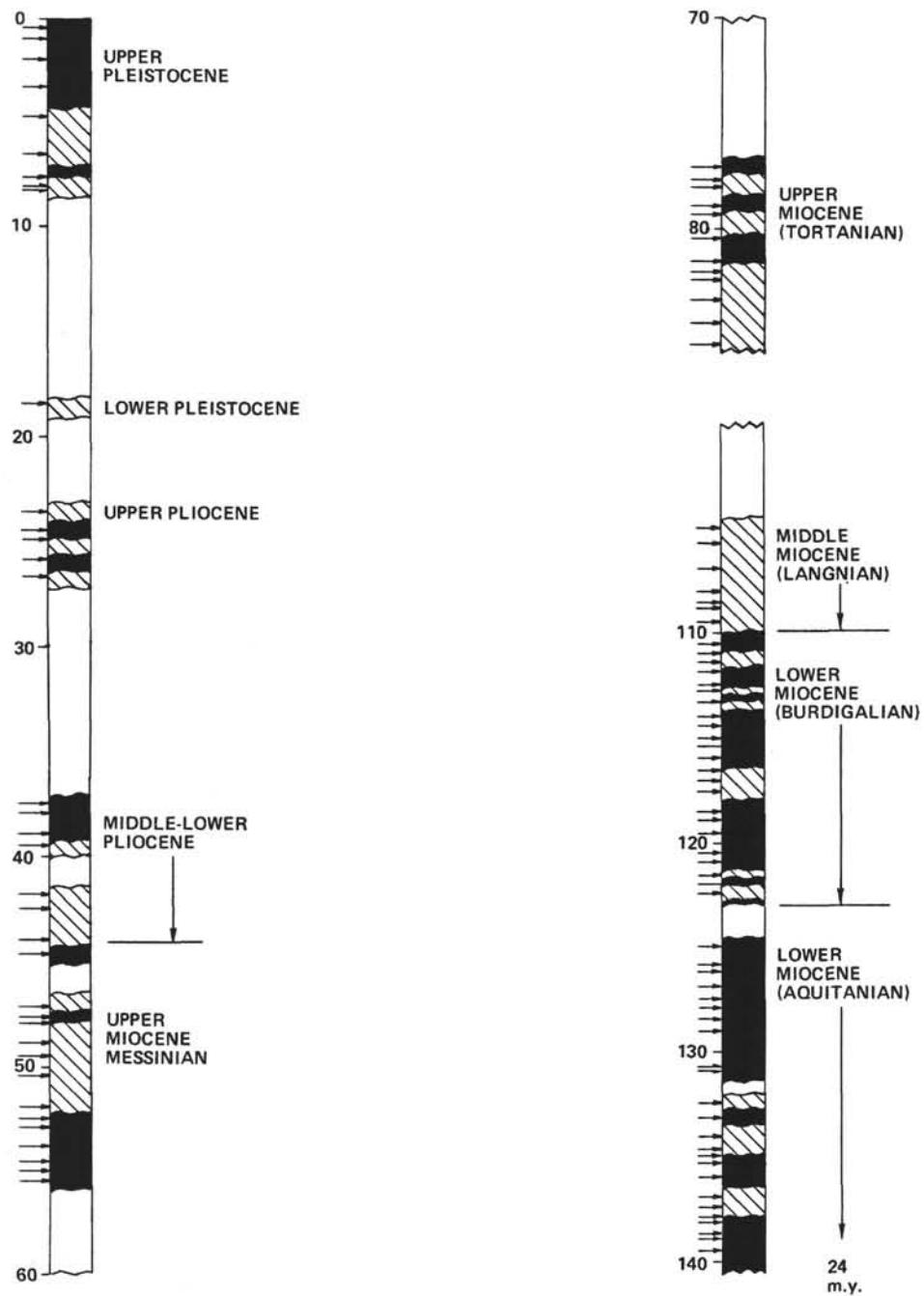


Figure 15. *Magnetic Stratigraphy of Site 15.*

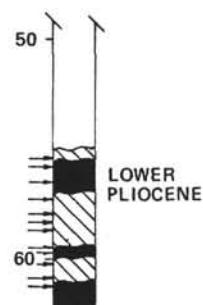
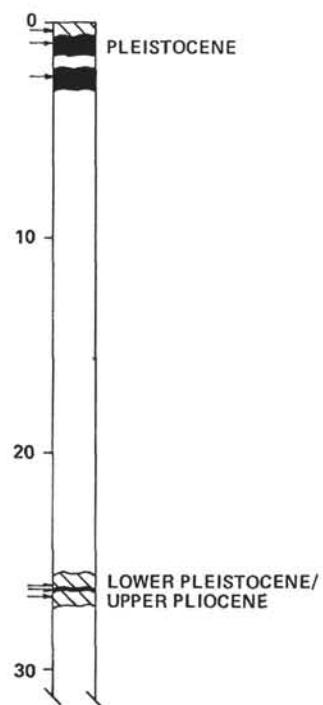


Figure 16. *Magnetic Stratigraphy of Site 16.*

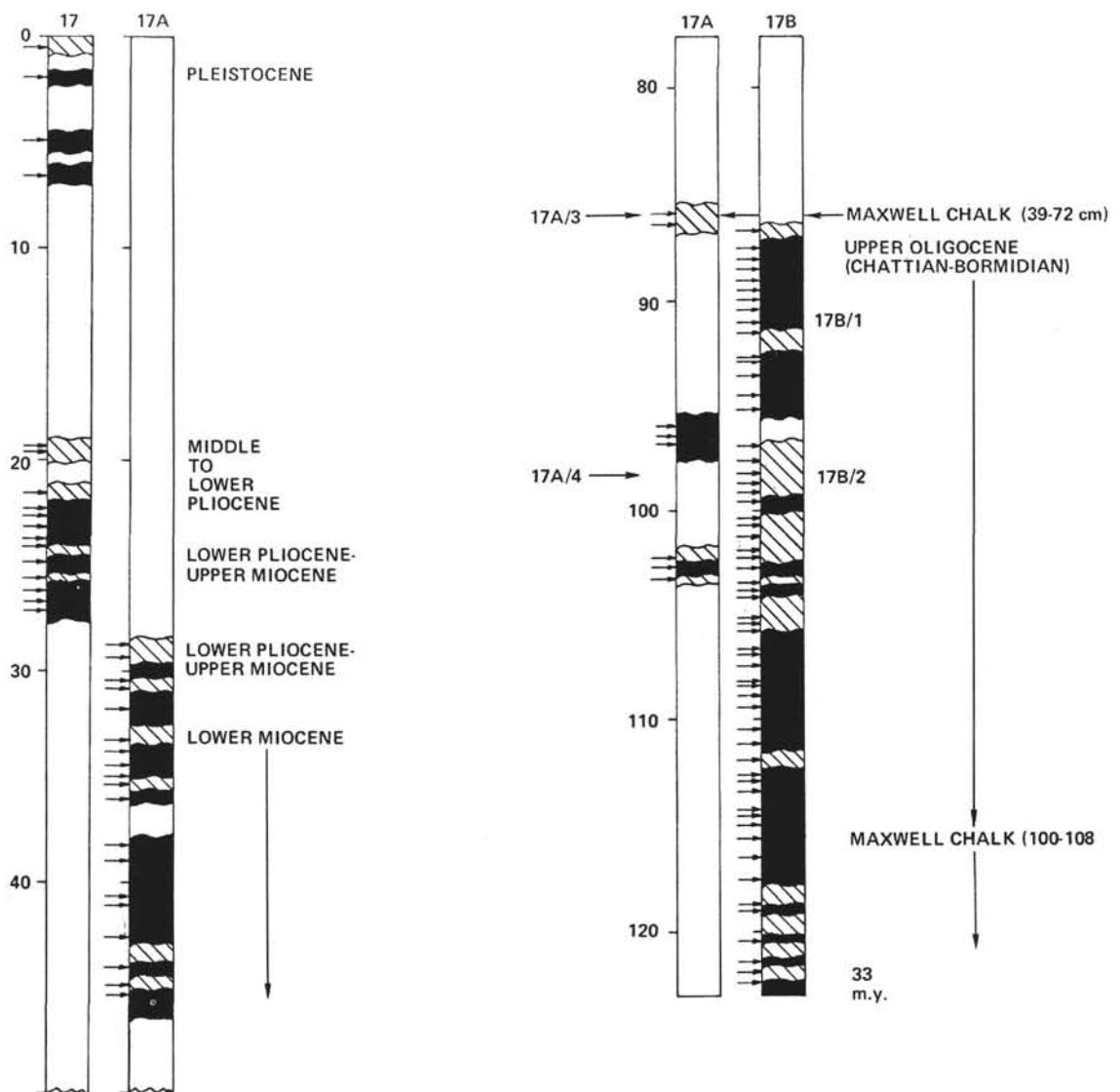


Figure 17. Magnetic Stratigraphy of Site 17.

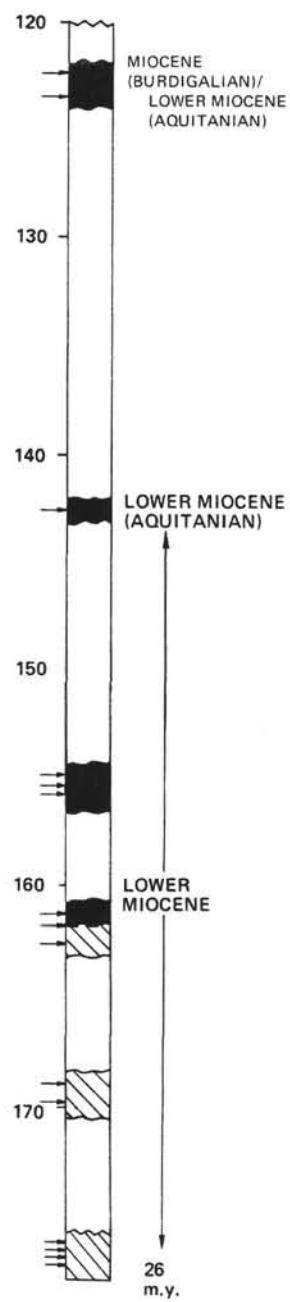


Figure 18. Magnetic Stratigraphy of Site 18.

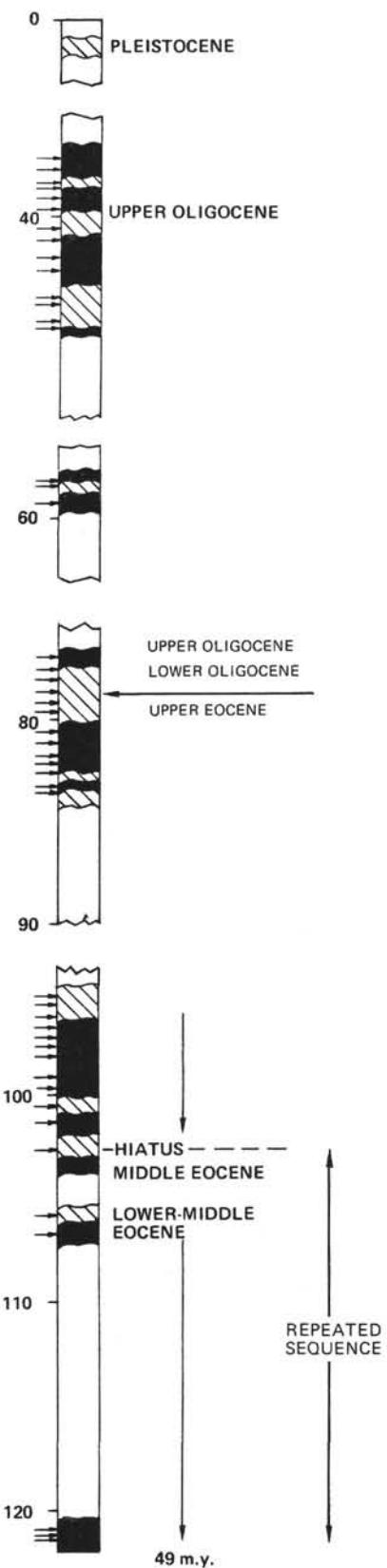


Figure 19. Magnetic Stratigraphy of Site 19.

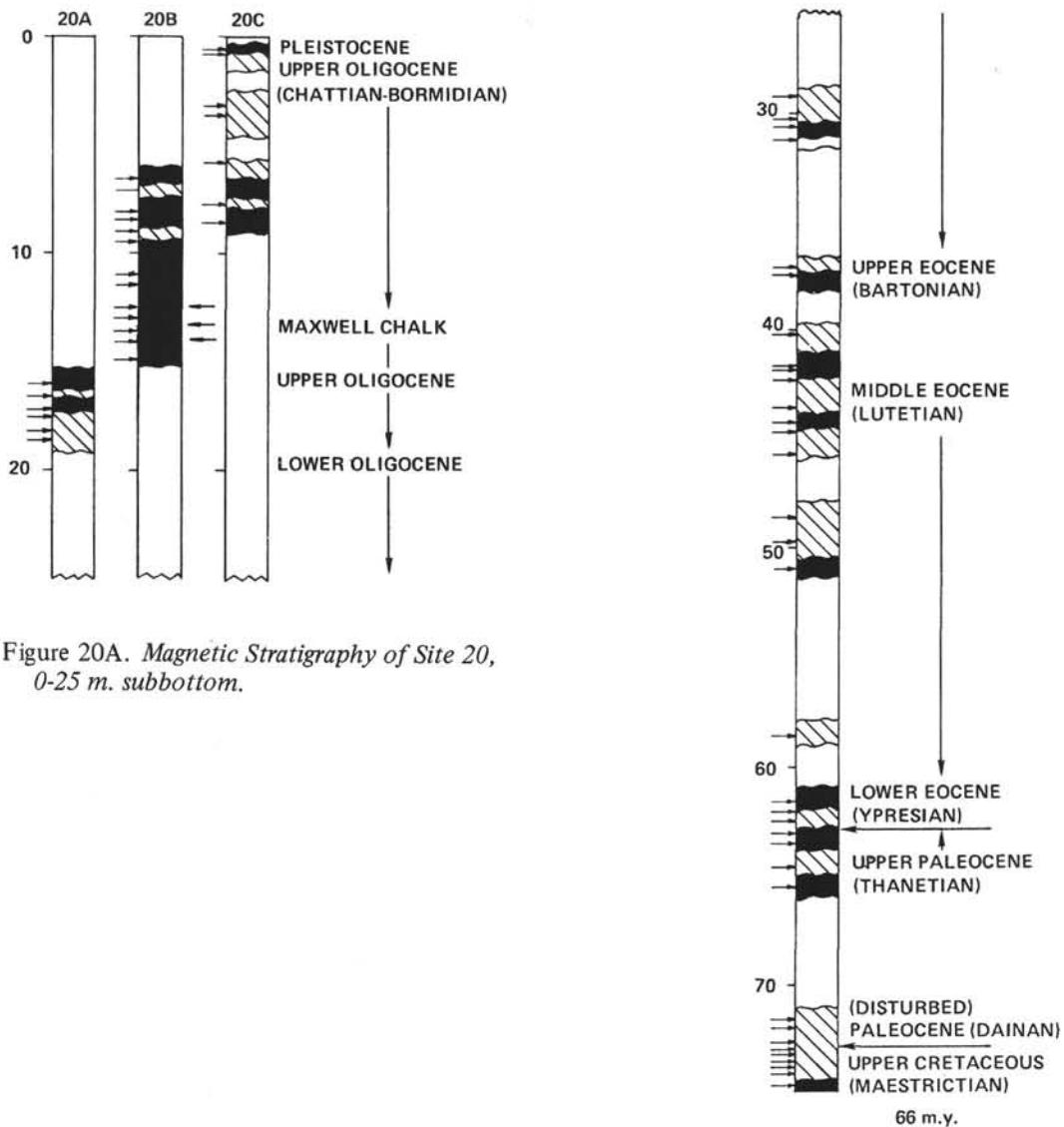


Figure 20A. *Magnetic Stratigraphy of Site 20, 0-25 m. subbottom.*

Figure 20B. *Magnetic Stratigraphy of Site 20, Hole 20C, 25 m - 75 m. subbottom.*